



# **Kingsway Solar Farm**

## **EIA Scoping Report**

**Appendices – Part 2**

**December 2024**

# APPENDIX E: GLINT AND GLARE RECEPTOR SCOPING STUDY

---

# Receptor Scoping and Methodology Document

Kingsway Solar Farm

October 2024



## PLANNING SOLUTIONS FOR:

- Solar
- Telecoms
- Railways
- Defence
- Buildings
- Wind
- Airports
- Radar
- Mitigation

[www.pagerpower.com](http://www.pagerpower.com)

## ADMINISTRATION PAGE

Job Reference:	12288B
Author:	[REDACTED]
Telephone:	[REDACTED]
Email:	[REDACTED]

Reviewed By:	[REDACTED]
Email:	[REDACTED]

Issue	Date	Detail of Changes
1	August 2024	Initial issue
2	October 2024	Update to include additional panel areas

[REDACTED]

[REDACTED]

Stour Valley Business Centre, Brundon Lane, Sudbury, CO10 7GB

T: +44 (0)1787 319001 E: [info@pagerpower.com](mailto:info@pagerpower.com) W: [www.pagerpower.com](http://www.pagerpower.com)

All aerial imagery (unless otherwise stated) is taken from Google Earth. Copyright © 2024 Google

## EXECUTIVE SUMMARY

### Report Purpose

Pager Power has been retained to assess the possible effects of glint and glare from a fixed ground-mounted solar photovoltaic development, located near Balsham, UK. This receptor scoping and methodology document shows the proposed receptors and the methodology that will be used to assess them in the glint and glare assessment, to be submitted as part of the Development Consent Order (DSO) application. The included receptors relate to road safety, residential amenity and aviation activity associated with Cambridge Airport, Duxford Aerodrome, Little Shelford Airfield, Newmarket Heath Airfield, Wooditton Airfield and Addenbrooke's Hospital Helipad.

### Report Summary

The receptors to be assessed within the glint and glare assessment to be submitted as part of the DCO application include aviation receptors associated with Cambridge Airport and Duxford Aerodrome, 2.2km of the A11, 6.5km of the B1052, 2.6km of Balsham /Cambridge Road, 6.5km of The Common, 6.3km of Common Road/Brinkley Road and 246 dwelling receptors.

### Guidance and Studies

Guidelines exist in the UK (produced by the Civil Aviation Authority) and in the USA (produced by the Federal Aviation Administration) with respect to solar developments and aviation activity. The UK CAA guidance is relatively high-level and does not prescribe a formal methodology.

A national policy for determining the impact of glint and glare on road safety, residential amenity and aviation safety has not been produced to date. Therefore, in the absence of this, Pager Power reviewed more general existing planning guidelines and the available studies (discussed below) in the process of defining its own glint and glare assessment guidance and methodology<sup>1</sup>. This methodology defines the process for determining the impact upon road safety, residential amenity and railway safety.

Pager Power's approach is to undertake geometric reflection calculations and, where a solar reflection is predicted, consider the screening (existing and/or proposed) between the receptor and the reflecting solar panels. The scenario in which a solar reflection can occur for all receptors is then identified and discussed, and a comparison is made against the available solar panel reflection studies to determine the overall impact.

---

<sup>1</sup> [Pager Power Glint and Glare Guidance](#), Fourth Edition (4.0), September 2022.

The available studies have measured the intensity of reflections from solar panels with respect to other naturally occurring and manmade surfaces. The results show that the reflections produced are of intensity similar to or less than those produced from still water and significantly less than reflections from glass and steel<sup>2</sup>. Reflections from solar panels are less intense than those from glass or steel because solar panels are designed in order to absorb light, rather than reflect it, as panels are more efficient when they reflect less light.

---

<sup>2</sup> SunPower, 2009, SunPower Solar Module Glare and Reflectance (appendix to Solargen Energy, 2010).

## LIST OF CONTENTS

Executive Summary .....	3
Report Purpose .....	3
Report Summary .....	3
Guidance and Studies .....	3
List of Contents .....	5
List of Figures .....	7
List of Tables .....	8
About Pager Power .....	9
1 Introduction .....	10
1.1 Overview .....	10
1.2 Pager Power's Experience .....	10
1.3 Glint and Glare Definition .....	10
2 Development Location and Details .....	11
2.1 Development Site .....	11
3 Glint and Glare Assessment Methodology .....	12
3.1 Guidance and Studies .....	12
3.2 Background .....	12
3.3 Methodology .....	12
3.4 Assessment Methodology and Limitations .....	13
4 Identification of Receptors .....	14
4.1 Aviation Receptors .....	14
4.2 Ground-Based Receptors Overview .....	24
4.3 Road Receptors .....	25
4.4 Dwelling Receptors .....	33
5 Geometric Assessment Methodology .....	41
5.1 Overview .....	41
5.2 Aviation Receptors .....	41

5.3	Road Receptors.....	43
5.4	Dwelling Receptors.....	44
5.5	Report Summary.....	44
Appendix A – Overview of Glint and Glare Guidance.....		45
	Overview.....	45
	UK Planning Policy.....	45
	Assessment Process – Ground-Based Receptors.....	47
	Aviation Assessment Guidance .....	48
	Civil Aviation Authority consolidation of UK Regulation 139/2014 .....	53
Appendix B – Overview of Glint and Glare Studies.....		54
	Overview.....	54
	Reflection Type from Solar Panels.....	54
	Solar Reflection Studies .....	55
Appendix C – Overview of Sun Movements and Relative Reflections.....		58
Appendix D – Glint and Glare Impact Significance .....		59
	Overview.....	59
	Impact Significance Definition.....	59
	Impact Significance Determination for ATC Tower .....	60
	Impact Significance Determination for Approaching Aircraft.....	61
	Impact Significance Determination for Road Receptors .....	62
	Impact Significance Determination for Dwelling Receptors .....	63
Appendix E – Reflection Calculations Methodology .....		64
	Pager Power Methodology .....	64
Appendix F – Assessment Limitations and Assumptions.....		66
	Pager Power’s Model.....	66
	Forge’s Sandia National Laboratories’ (SGHAT) Model.....	68



## LIST OF FIGURES

Figure 1 Development site boundary overlaid onto aerial imagery .....	11
Figure 2 Aerodrome chart for Cambridge Airport.....	15
Figure 3 Runway approach paths (blue lines) – aerial image .....	16
Figure 4 Location of the ATC Tower within Cambridge Airport.....	17
Figure 5 Ground-based view of the ATC Tower at Cambridge Airport (visual control room circled) .....	17
Figure 6 Splayed approach and final sections of visual circuits.....	18
Figure 7 Determined circuit for runway 06/24 .....	19
Figure 8 Duxford Aerodrome aviation receptors (light blue lines) – aerial image .....	20
Figure 9 Location of the ATC Tower within Cambridge Airport.....	21
Figure 10 Ground-based view of the ATC Tower at Duxford Aerodrome (visual control room circled) .....	21
Figure 11 Assessed aerodromes relative to the proposed development .....	22
Figure 12 Locations of the aerodromes to be assessed at high-level relative to the development .....	23
Figure 13 Assessment area .....	24
Figure 14 Road receptors A1 to A19 .....	26
Figure 15 Road receptors A20 to A24 .....	27
Figure 16 Road receptors B1 to B23 .....	28
Figure 17 Road receptors B24 to B55.....	28
Figure 18 Road receptors B55 to B56.....	29
Figure 19 Road receptors C1 to C27 .....	29
Figure 20 Road receptors D1 to D30 .....	30
Figure 21 Road receptors D31 to D53.....	30
Figure 22 Road receptors D54 to D66.....	31
Figure 23 Road receptors E1 to E23.....	31
Figure 24 Road receptors E24 to E45 .....	32
Figure 25 Road receptors E46 to E64 .....	32

Figure 26 Overview of all dwellings.....	33
Figure 27 Dwellings 1 to 13.....	34
Figure 28 Dwellings 14 to 18.....	34
Figure 29 Dwellings 19 to 43.....	35
Figure 30 Dwellings 44 to 46.....	35
Figure 31 Dwellings 47 to 62.....	36
Figure 32 Dwellings 63 to 109.....	36
Figure 33 Dwellings 110 to 149.....	37
Figure 34 Dwellings 150 to 172.....	37
Figure 35 Dwellings 173 to 177.....	38
Figure 36 Dwellings 178 to 195.....	38
Figure 37 Dwellings 196 to 235.....	39
Figure 38 Dwellings 236 to 237.....	39
Figure 39 Dwellings 238 to 246.....	40

## LIST OF TABLES

Table 1 Summary of identified road receptors.....	25
---	----

## ABOUT PAGER POWER

Pager Power is a dedicated consultancy company based in Suffolk, UK. The company has undertaken projects in 59 countries within Europe, Africa, America, Asia and Australasia.

The company comprises a team of experts to provide technical expertise and guidance on a range of planning issues for large and small developments.

Pager Power was established in 1997. Initially the company focus was on modelling the impact of wind turbines on radar systems. Over the years, the company has expanded into numerous fields including:

- Renewable energy projects;
- Building developments;
- Aviation and telecommunication systems.

Pager Power prides itself on providing comprehensive, understandable and accurate assessments of complex issues in line with national and international standards. This is underpinned by its custom software, longstanding relationships with stakeholders and active role in conferences and research efforts around the world.

Pager Power's assessments withstand legal scrutiny and the company can provide support for a project at any stage.

## 1 INTRODUCTION

### 1.1 Overview

Pager Power has been retained to assess the possible effects of glint and glare from a fixed ground-mounted solar photovoltaic development, located near Balsham, UK. This receptor scoping and methodology document shows the proposed receptors and the methodology that will be used to assess them in the glint and glare assessment, to be submitted as part of the Development Consent Order (DSO) application. The included receptors relate to road safety, residential amenity and aviation activity associated with Cambridge Airport, Duxford Aerodrome, Little Shelford Airfield, Newmarket Heath Airfield, Wooditton Airfield and Addenbrooke's Hospital Helipad.

This report contains the following:

- Solar development details;
- Explanation of glint and glare;
- Overview of relevant guidance and relevant studies;
- Overview of sun movement;
- Assessment methodology;
- Identification of receptors.

### 1.2 Pager Power's Experience

Pager Power has undertaken over 1,400 glint and glare assessments in the UK and internationally. The studies have included assessment of civil and military aerodromes, railway infrastructure and other ground-based receptors including roads and dwellings.

### 1.3 Glint and Glare Definition

The definition<sup>3</sup> of glint and glare is as follows:

- Glint – a momentary flash of bright light typically received by moving receptors or from moving reflectors;
- Glare – a continuous source of bright light typically received by static receptors or from large reflective surfaces.

The term 'solar reflection' is used in this report to refer to both reflection types i.e. glint and glare.

---

<sup>3</sup> These definitions are aligned with those presented within the National Policy Statement for Renewable Energy Infrastructure (EN-3) – published by the Department for Energy Security and Net Zero January 2024 and the Federal Aviation Administration in the USA.

## 2 DEVELOPMENT LOCATION AND DETAILS

### 2.1 Development Site

Figure 1 below shows the development site boundary overlaid onto aerial imagery as the red areas. No solar panel layout has yet been determined, this assessment has assumed maximum coverage within the site boundary, this is the most conservative approach.



Figure 1 Development site boundary overlaid onto aerial imagery

## 3 GLINT AND GLARE ASSESSMENT METHODOLOGY

### 3.1 Guidance and Studies

Appendices A and B present a review of relevant guidance and independent studies with regard to glint and glare issues from solar panels. The overall conclusions from the available studies are as follows:

- Specular reflections of the sun from solar panels are possible;
- The measured intensity of a reflection from solar panels can vary from 2% to 30% depending on the angle of incidence;
- Published guidance shows that the intensity of solar reflections from solar panels are equal to or less than those from water. It also shows that reflections from solar panels are significantly less intense than many other reflective surfaces, which are common in an outdoor environment.

### 3.2 Background

Details of the Sun's movements and solar reflections are presented in Appendix C.

### 3.3 Methodology

#### 3.3.1 Pager Power's Methodology

The glint and glare assessment methodology has been derived from the information provided to Pager Power through consultation with stakeholders and by reviewing the available guidance and studies. The methodology for this glint and glare assessment is as follows:

- Identify receptors in the area surrounding the solar development;
- Consider direct solar reflections from the solar development towards the identified receptors by undertaking geometric calculations;
- Consider the visibility of the panels from the receptor's location. If the panels are not visible from the receptor then no reflection can occur;
- Based on the results of the geometric calculations, determine whether a reflection can occur, and if so, at what time it will occur;
- Consider both the solar reflection from the solar development and the location of the direct sunlight with respect to the receptor's position;
- Consider the solar reflection with respect to the published studies and guidance - including intensity calculations where appropriate;
- Determine whether a significant detrimental impact is expected in line with the process presented in Appendix D.

### **3.3.2 Sandia National Laboratories' Methodology**

Sandia National Laboratories developed the Solar Glare Hazard Analysis Tool (SGHAT) which is no longer freely available however it is now developed by Forge Solar. Pager Power uses this model where required for aviation receptors. Whilst strictly applicable in the USA and to solar photovoltaic developments only, the methodology is widely used by aviation stakeholders internationally.

### **3.4 Assessment Methodology and Limitations**

Further technical details regarding the methodology of the geometric calculations and limitations are presented in Appendix E and F.

## 4 IDENTIFICATION OF RECEPTORS

### 4.1 Aviation Receptors

The following subsections present the relevant data and receptors associated with the assessed airfields. The locations of the airfields that are to be assessed relative to the proposed development are shown in Figure 11 on page 21, and summarised below:

- Cambridge Airport: approximately 8.4km north-west of the development;
- Duxford Aerodrome: approximately 8.6km south-west of the development.

Three further airfields have been identified to be assessed at a high-level. It is considered due to their distance from the development, and their runway configurations, that no more than a low impact is possible. The locations of the airfields relative to the development are shown in Figure 12 on page 22, and summarised below:

- Little Shelford Airfield: approximately 7.4km south-west of the development;
- Newmarket Heath Airfield: approximately 7.9km north-east of the development;
- Woodditton Airfield: approximately 8.8km north-east of the development, and;
- Addenbrooke's Hospital Helipad: approximately 7.3km west of the development.

#### 4.1.1 Cambridge Airport Information

Cambridge Airport is a Civil Aviation Authority (CAA) licenced airport and is understood to have an Air Traffic Control (ATC) Tower. It has one operational runway, the details<sup>4</sup> of which are presented below:

- 05/23 measuring 1,964m by 45m (asphalt);
- 05G/23G measuring 900m by 35m (grass).

The aerodrome chart for Cambridge Airport<sup>9</sup> is shown in Figure 2, on the following page.

This runway has two associated approach paths, one for each bearing. It is Pager Power's methodology to assess whether a solar reflection can be experienced on the approach paths for the associated runways. This is considered to be the most critical stage of the flight.

A geometric glint and glare assessment has been undertaken for the approach and departure paths for runway 05/23. Locations have been selected every 0.1-miles along the extended runway centre line from 50ft above the runway threshold out to a distance of 2-miles. The height of the aircraft is determined by using a 3-degree descent path relative to the runway threshold height.

Figure 3 on page 16, shows the assessed aircraft approach paths, and ATC Tower.

---

<sup>4</sup> NATS AIP



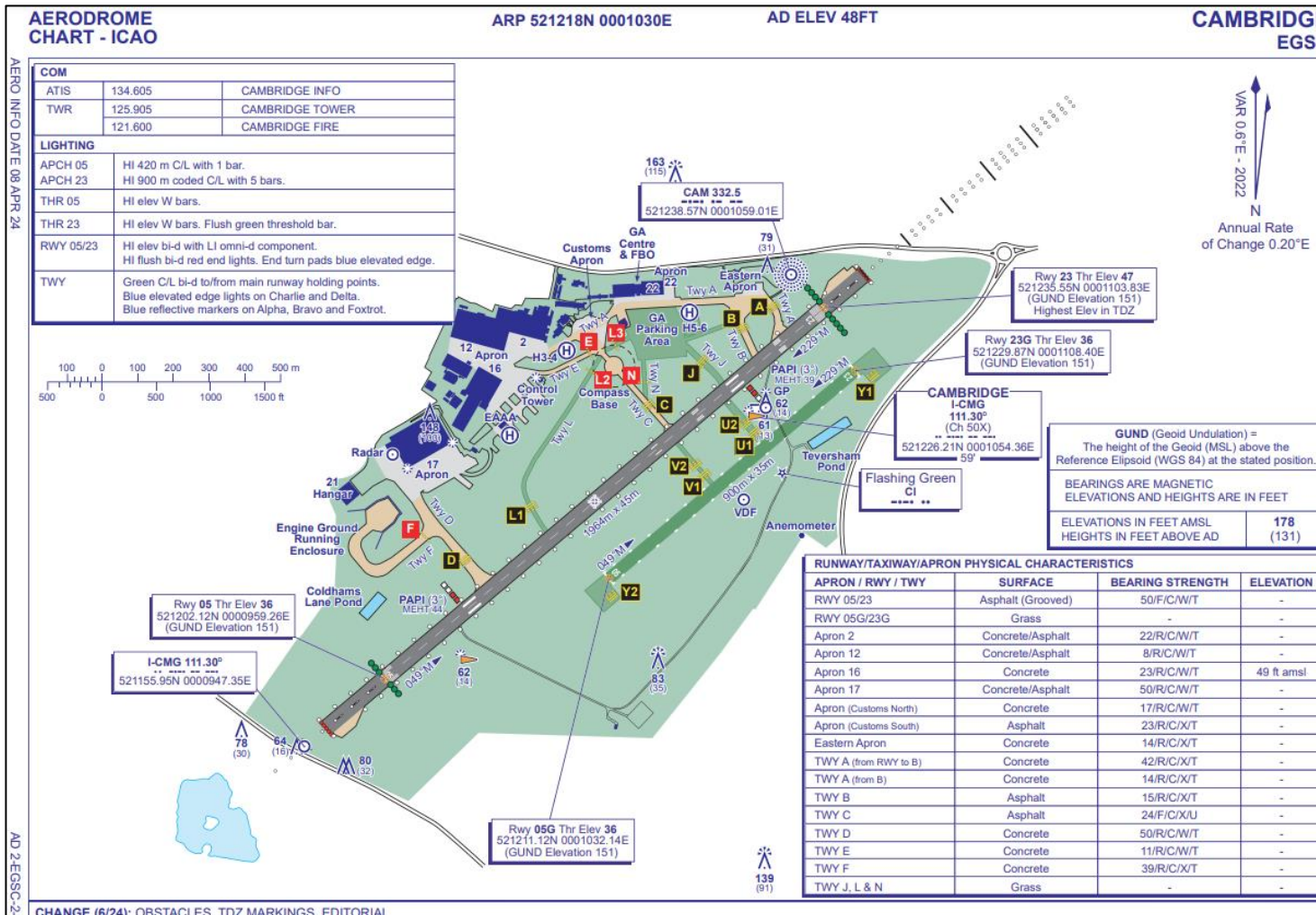


Figure 2 Aerodrome chart for Cambridge Airport



Figure 3 Runway approach paths (blue lines) – aerial image

Cambridge Airport has an ATC Tower, which is 24m tall (agl) and located approximately 0.9km north-east of the runway 05 threshold. The location of the ATC Tower is shown in Figure 4 below, and ground-based views of the ATC Tower are shown in Figure 5 below.



Figure 4 Location of the ATC Tower within Cambridge Airport



Figure 5 Ground-based view of the ATC Tower at Cambridge Airport (visual control room circled)

#### 4.1.2 Duxford Aerodrome Information

Duxford Aerodrome is an unlicensed aerodrome and is understood to have an ATC Tower. It has two operational runways, the details<sup>5</sup> of which are presented below:

- 06R/24L measuring 1,448m by 32m (grass);
- 06L/24R measuring 882m by 25m (grass).

Duxford Aerodrome is a General Aviation (GA) airfield where aviation activity is dynamic and does not necessarily follow the typical approaches / flight paths of a larger licensed aerodrome or airport. It is not possible to assess every single location of airspace that an aircraft travels in flight around an aerodrome; however, it is possible to assess the most frequently flown flight paths and the most critical stages of flight, which would cover most, or all, of the relevant locations.

As such, Pager Power's methodology is to assess whether a solar reflection can be experienced on a 5-degree splayed approach path based on the extended runway centreline, and the final sections of the visual circuits and joins on approach to the corresponding runway thresholds.

The assessed receptors are based on the following characteristics:

- 1-mile approach path with a splay angle of 5 degrees, considering 2.5 degrees either side of the extended runway centreline;
- A descent angle of 5 degrees;
- Circuit width of 1 nautical mile from runway centreline;
- Maximum altitude of 500 feet above the aerodrome threshold altitude.

Figure 6 below illustrates the splayed approach and final sections of the visual circuits.

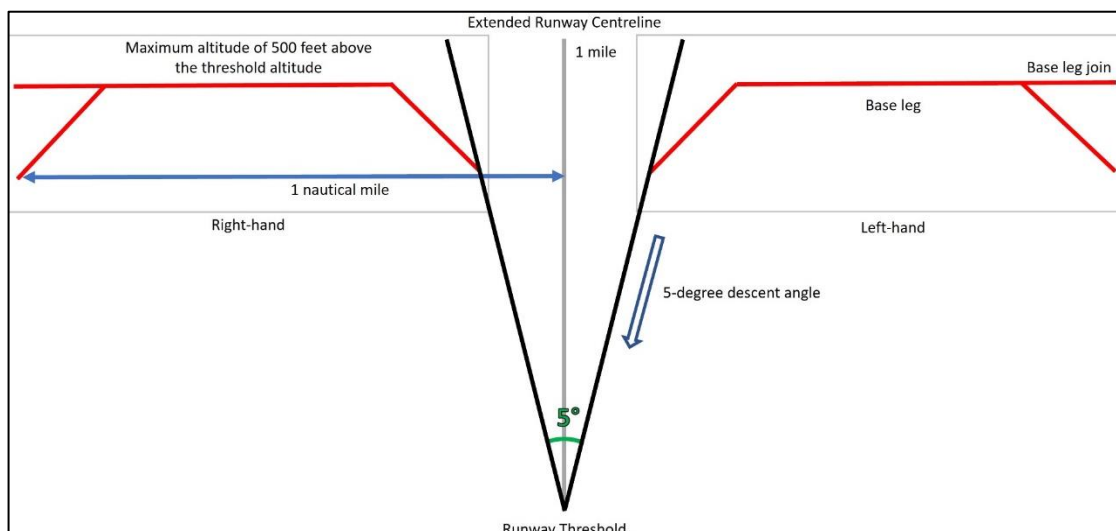


Figure 6 Splayed approach and final sections of visual circuits

<sup>5</sup> Pooleys Flight Guide, 61<sup>st</sup> Edition

Duxford Aerodrome has a defined circuit for runway 06/24, this is shown in Figure 7 below<sup>6</sup>. The circuit will be assessed with receptor points every 0.2 miles with a descent angle of 5° and a maximum altitude of 1,000ft above the aerodrome threshold.

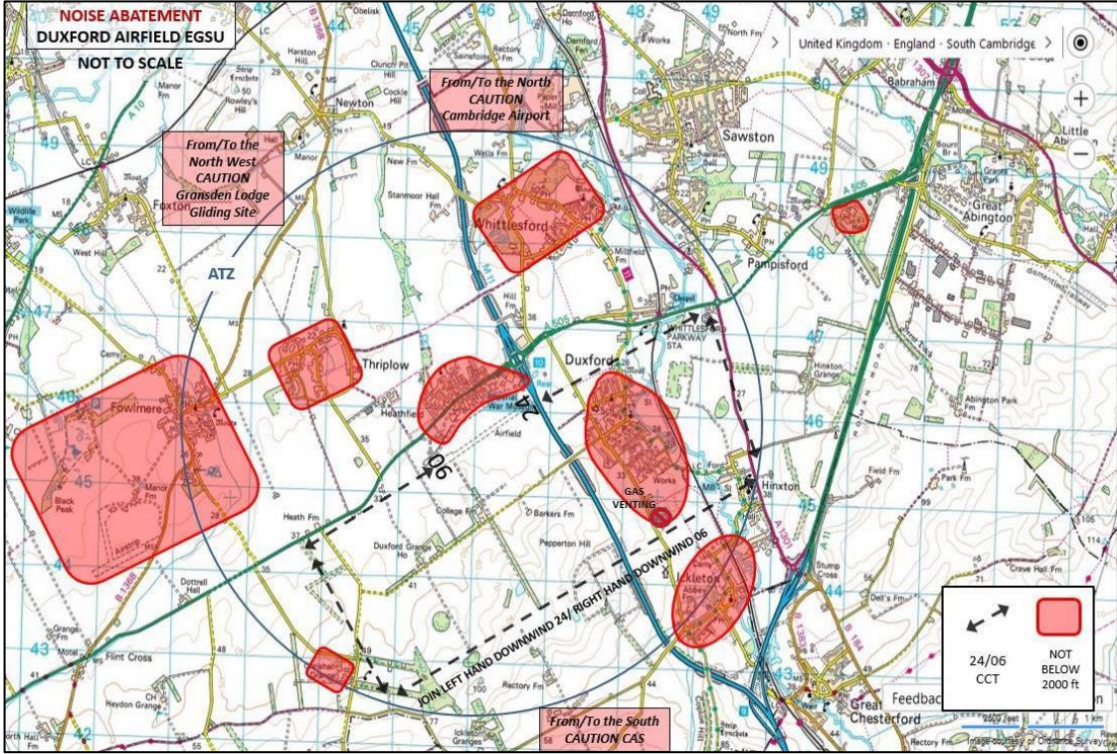


Figure 7 Determined circuit for runway 06/24

Figure 8 on the following page illustrates the assessed splayed approach for runways 05L/25R and 05R/25L at Duxford Aerodrome, and the 05RH/23LH visual circuit.

<sup>6</sup> Source: <https://www.iwm.org.uk/sites/default/files/files/2024-05/Duxford%20information%20for%20pilots%202024.pdf> (accessed 28/08/2024)



Figure 8 Duxford Aerodrome aviation receptors (light blue lines) – aerial image

Duxford Aerodrome has an ATC Tower, which is 9m tall<sup>7</sup> (agl) and located approximately 0.9km north-east of the runway 05L threshold. The location of the ATC Tower is shown in Figure 9 below, and ground-based views of the ATC Tower are shown in Figure 10 below.



Figure 9 Location of the ATC Tower within Cambridge Airport



Figure 10 Ground-based view of the ATC Tower at Duxford Aerodrome (visual control room circled)

---

<sup>7</sup>Determined through available imagery



Figure 11 Assessed aerodromes relative to the proposed development

#### 4.1.3 Newmarket Heath Airfield Information

Newmarket Heath Airfield is an unlicensed aerodrome and is understood not to have an ATC Tower. It has one operational runway, the details<sup>6</sup> of which are presented below, and one helicopter landing zone:

- 14/32 measuring 914m by 70m (grass).

#### 4.1.4 Woodditton Airfield Information

Woodditton Airfield is an unlicensed aerodrome and is understood not to have an ATC Tower. It has one operational runway, the details<sup>7</sup> of which are presented below:

- 05/23 measuring 460m by 14m (grass).

#### 4.1.5 Little Shelford Airfield Information

Little Shelford Airfield is an unlicensed aerodrome and is understood not to have an ATC Tower. It has one operational runway, the details<sup>7</sup> of which are presented below:

- 05/23 measuring 615m by 20m (grass).

#### 4.1.6 High-Level Aviation

Figure 12 on the following page show the locations of the airfields to be assessed at a high-level, relative to the development. They also show the splayed runway approach paths at each airfield runway, and the 2-mile approach paths for each helicopter landing zone.





Figure 12 Locations of the aerodromes to be assessed at high-level relative to the development

## 4.2 Ground-Based Receptors Overview

There is no formal guidance with regard to the maximum distance at which glint and glare should be assessed. From a technical perspective, there is no maximum distance for potential reflections. The significance of a reflection however decreases with distance because the proportion of an observer's field of vision that is taken up by the reflecting area diminishes as the separation distance increases. Terrain and shielding by vegetation are also more likely to obstruct an observer's view at longer distances.

A 1km assessment area is considered appropriate for glint and glare effects on ground-based receptors. Receptors within this distance are identified based on mapping and aerial photography of the region. The assessment area is bounded by the yellow outline in Figure 13 below. Receptors to the north of the development are not included because solar reflections would not be geometrically possible towards the north when the azimuth angle is considered<sup>8</sup>.

The receptor details are presented in Appendix G and the terrain elevations have been interpolated based on OS Terrain 50 DTM<sup>9</sup> data.

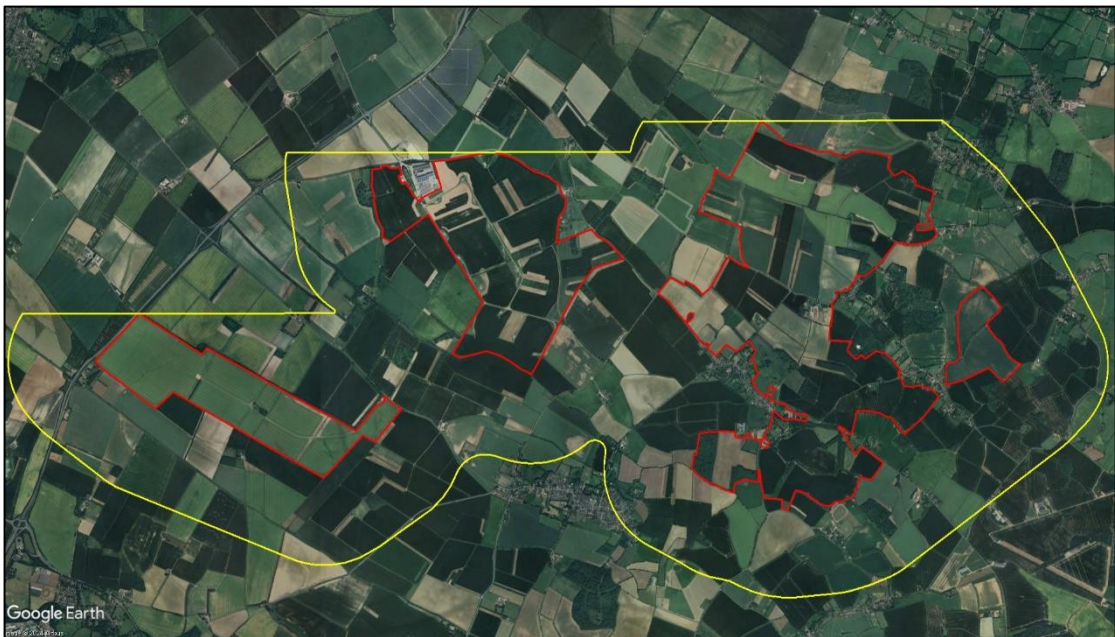


Figure 13 Assessment area

---

<sup>8</sup> For fixed, south-facing panels at this latitude, reflections towards ground-based receptors located further north than any proposed panel are highly unlikely

<sup>9</sup> Digital Terrain Model

## 4.3 Road Receptors

### 4.3.1 Road Receptors Overview

Road types can generally be categorised as:

- Major National – Typically a road with a minimum of two carriageways with a maximum speed limit of up to 70mph. These roads typically have fast moving vehicles with busy traffic;
- National – Typically a road with one or more carriageways with a maximum speed limit 60mph or 70mph. These roads typically have fast moving vehicles with moderate to busy traffic density;
- Regional – Typically a single carriageway with a maximum speed limit of up to 60mph. The speed of vehicles will vary with a typical traffic density of low to moderate;
- Local – Typically roads and lanes with the lowest traffic densities. Speed limits vary.

Technical modelling is not recommended for local roads, where traffic densities are likely to be relatively low. Any solar reflections from the development that are experienced by a road user along a local road would be considered low impact in the worst case in accordance with the guidance presented in Appendix D. The analysis has therefore considered major national, national, and regional roads that:

- Are within the one-kilometre assessment area;
- Have a potential view of the panels.

### 4.3.2 Identified Road Receptors

Table 1 below shows a summary of the roads identified within the 1km assessment area. Receptors are placed circa 100m apart. A height of 1.5 metres above ground level has been taken as the typical eye level of a road user<sup>10</sup>. Figures 14 to 25, on the following pages show the assessed road receptors.

Road	Receptors
A11	A1 – A24
B1052	B1 – B28
Balsham Road/Cambridge Road	C1 – C27
The Common	D1 – D66
Common Road/Brinkley Road	E1 – E64

Table 1 Summary of identified road receptors

<sup>10</sup> This fixed height for the road receptors is for modelling purposes. Changes to the modelling height by a few metres is not expected to significantly change the modelling results. Views for elevated drivers are also considered in the results discussion, where appropriate.

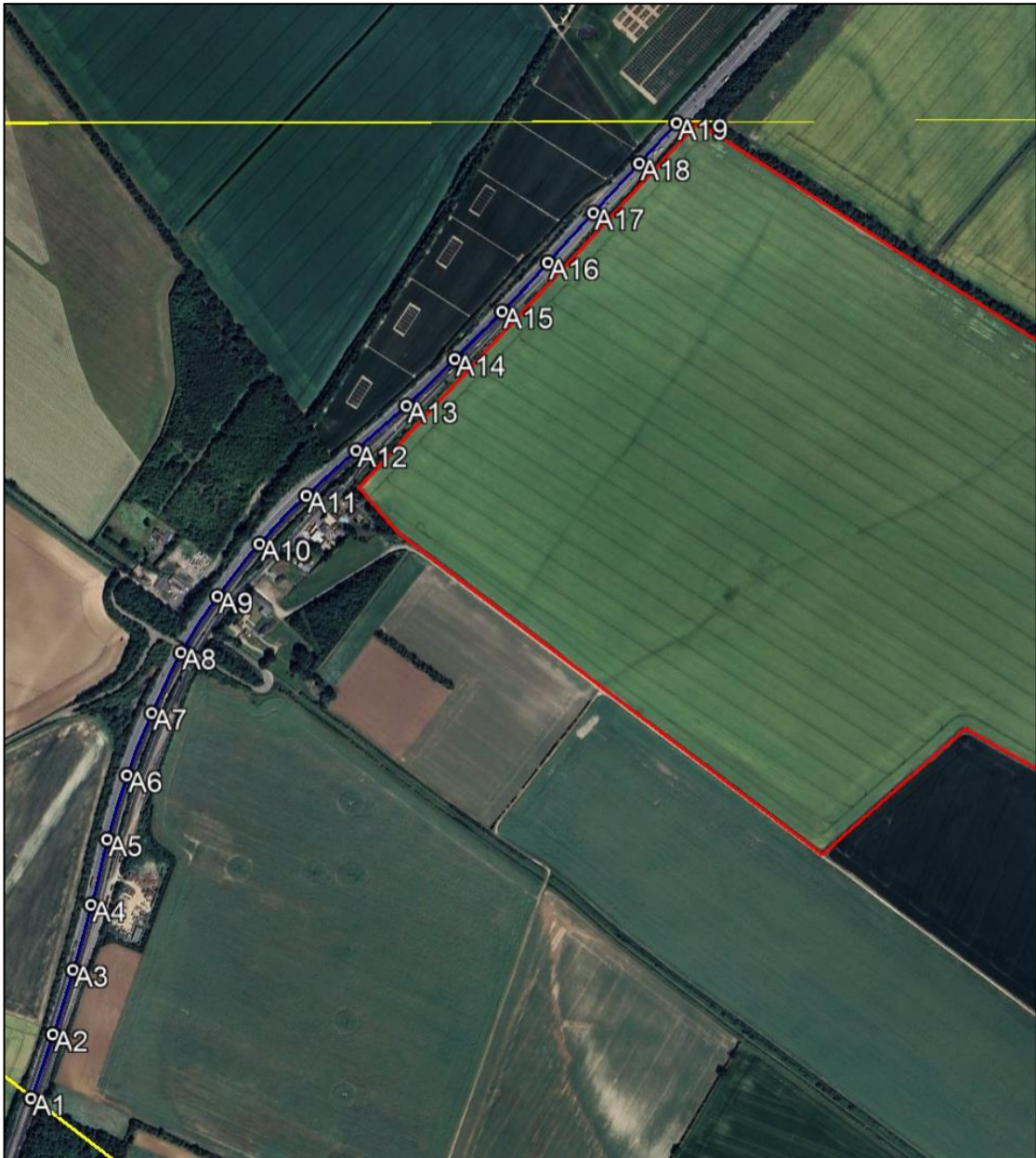


Figure 14 Road receptors A1 to A19



Figure 15 Road receptors A20 to A24



Figure 16 Road receptors B1 to B23



Figure 17 Road receptors B24 to B55



Figure 18 Road receptors B55 to B56



Figure 19 Road receptors C1 to C27

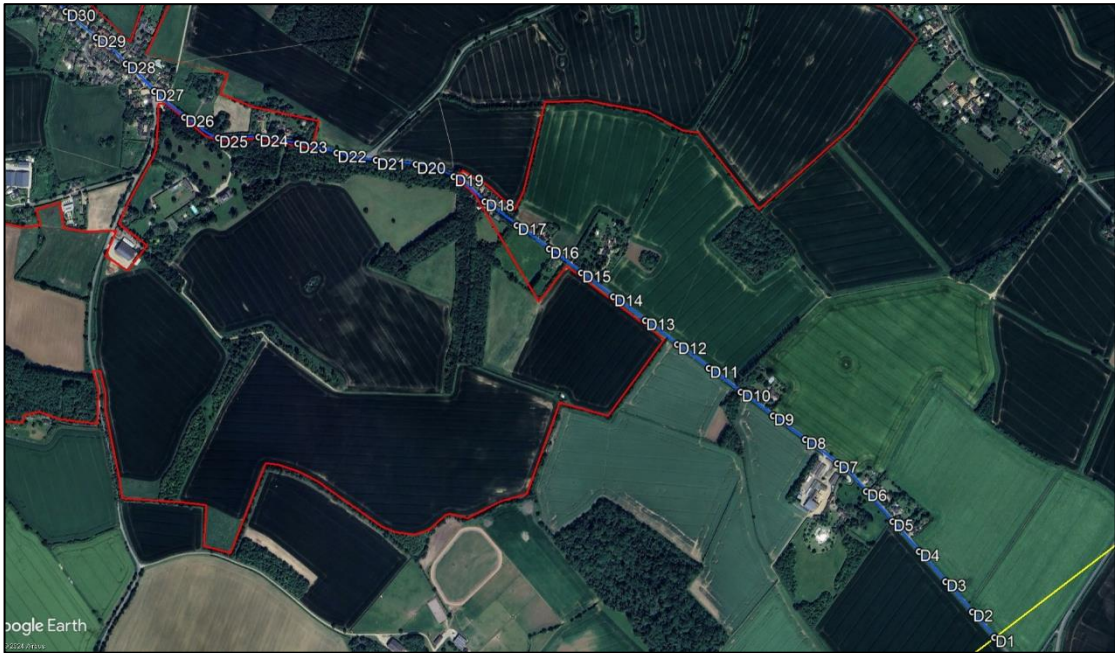


Figure 20 Road receptors D1 to D30

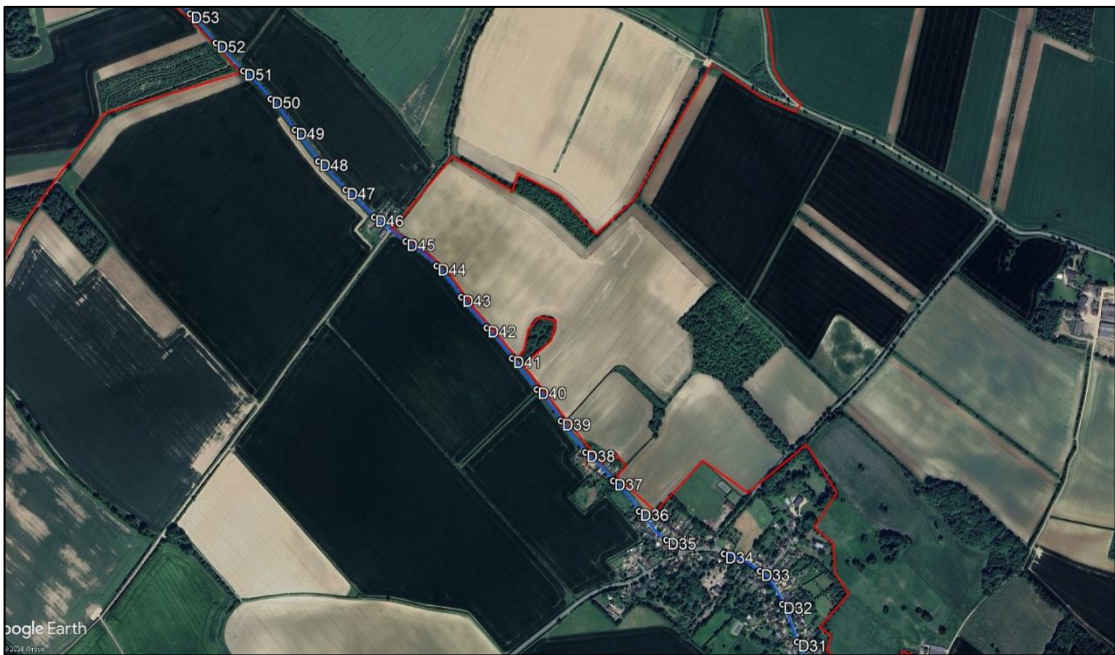


Figure 21 Road receptors D31 to D53



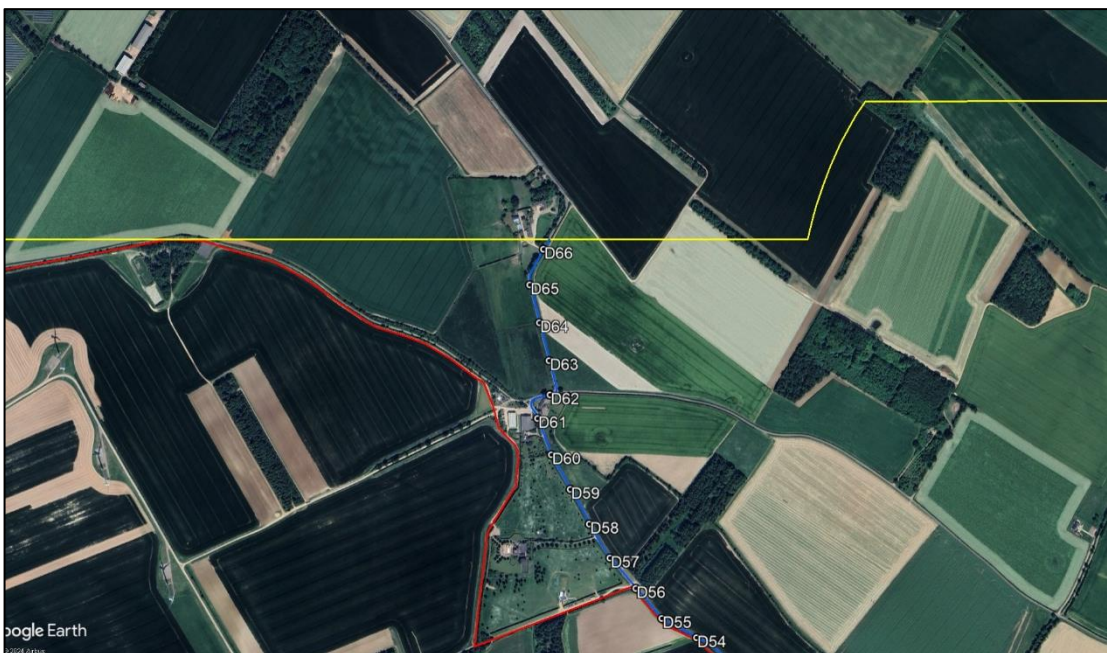


Figure 22 Road receptors D54 to D66

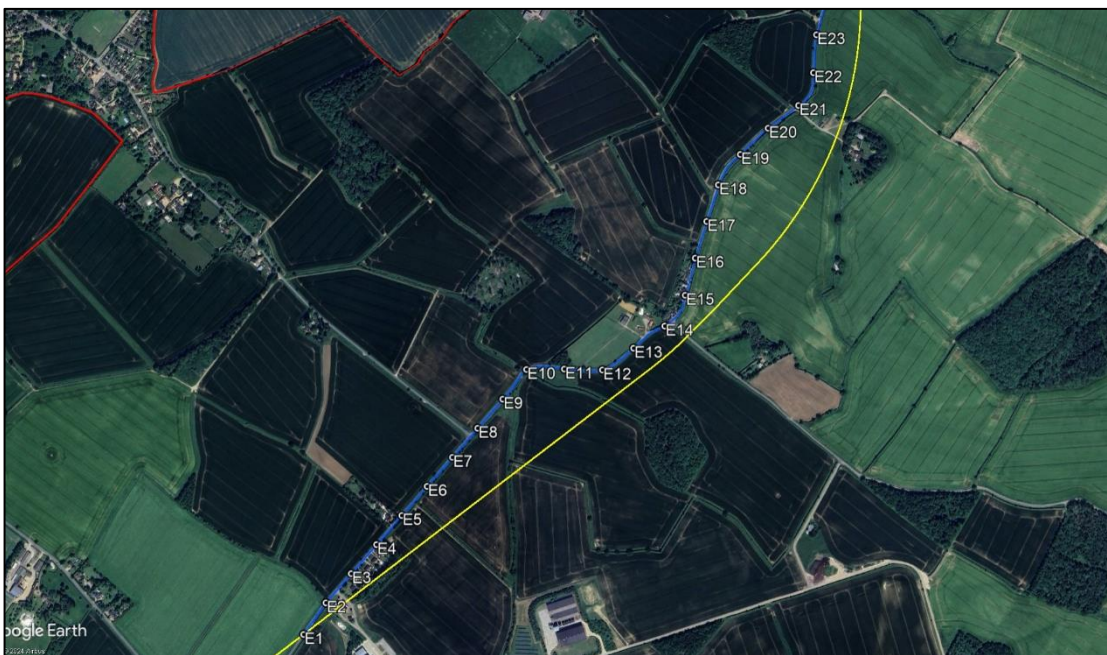


Figure 23 Road receptors E1 to E23



Figure 24 Road receptors E24 to E45



Figure 25 Road receptors E46 to E64

## 4.4 Dwelling Receptors

### 4.4.1 Dwelling Receptors Overview

The analysis has considered dwellings that:

- Are within the one-kilometre assessment area; and
- Have a potential view of the panels.

In residential areas with multiple layers of dwellings, only the outer dwellings have been considered for assessment. This is because they will mostly obscure views of the solar panels to the dwellings behind them, which will therefore not be impacted by the development because line of sight will be removed, or they will experience comparable effects to the closest assessed dwelling.

Additionally, in some cases, a single receptor point may be used to represent a small number of separate addresses. In such cases, the results for the receptor will be representative of the adjacent observer locations, such that the overall level of effect in each area is captured reliably.

### 4.4.2 Identified Dwelling Receptors

The assessed dwelling receptors are shown in Figures 25 to 39, below and on the following pages. In total, 246 dwelling receptors will be assessed. An additional 1.8m height above ground is used in the modelling to simulate the typical viewing height of an observer on the ground floor<sup>11</sup>.



Figure 26 Overview of all dwellings

<sup>11</sup> This fixed height for the dwelling receptors is for modelling purposes. Changes to the modelling height by a few metres is not expected to significantly change the modelling results. Views above ground floor are considered in the results discussion where necessary.



Figure 27 Dwellings 1 to 13

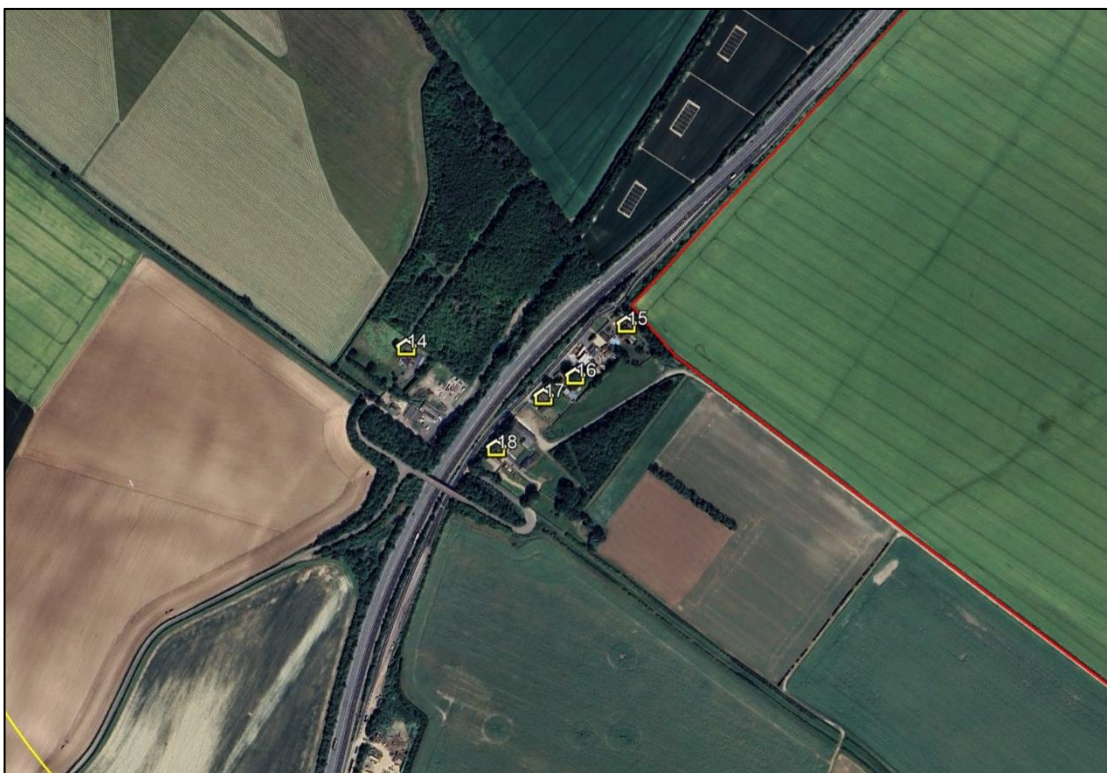


Figure 28 Dwellings 14 to 18



Figure 29 Dwellings 19 to 43



Figure 30 Dwellings 44 to 46



Figure 31 Dwellings 47 to 62



Figure 32 Dwellings 63 to 109



Figure 33 Dwellings 110 to 149



Figure 34 Dwellings 150 to 172

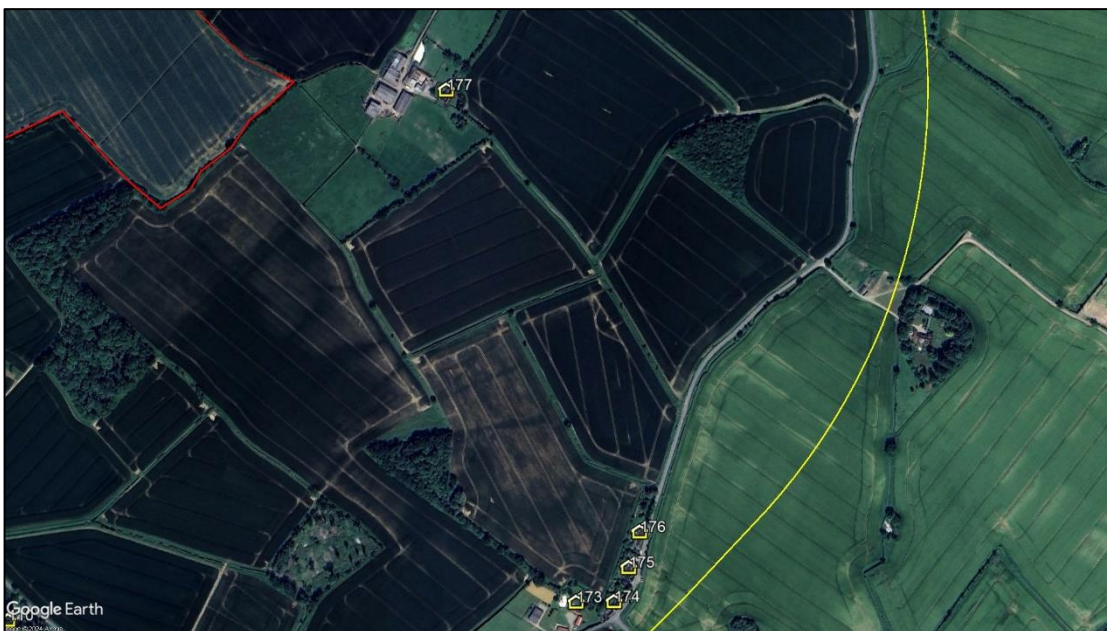


Figure 35 Dwellings 173 to 177



Figure 36 Dwellings 178 to 195





Figure 37 Dwellings 196 to 235

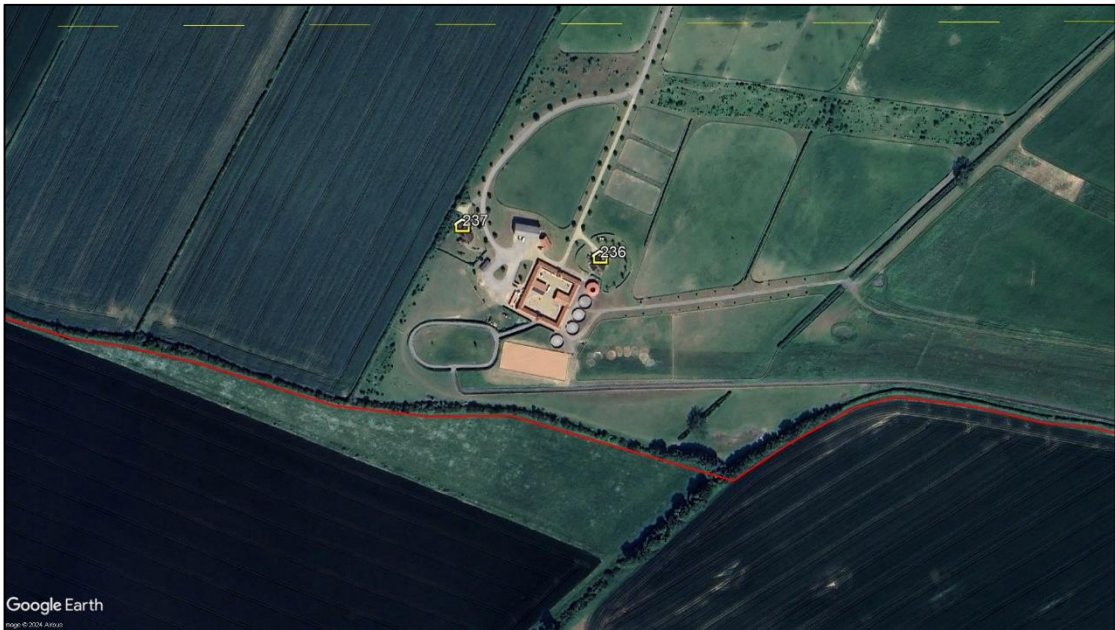


Figure 38 Dwellings 236 to 237



Figure 39 Dwellings 238 to 246

## 5 GEOMETRIC ASSESSMENT METHODOLOGY

### 5.1 Overview

The following sub-section presents the methodology used to assess each receptor type, with the relevant criteria set out in each sub-section. The criteria are determined by the assessment process for each receptor, which are set out in Appendix D.

When determining the visibility of the reflecting panels for an observer, a conservative review of the available imagery is used, whereby it is assumed views of the panels are possible if it cannot be reliably determined that existing screening will remove effects.

### 5.2 Aviation Receptors

The process for quantifying impact significance is defined in the report appendices. For the runway approach paths, the key considerations are:

- Whether a reflection is predicted to be experienced in practice.
- The location of glare relative to a pilot's primary field-of-view (50 degrees either side of the approach bearing).
- The intensity of glare for the solar reflections:
  - Glare with 'low potential for temporary after-image' (green glare);
  - Glare with 'potential for temporary after-image' (yellow glare);
  - Glare with 'potential for permanent eye damage' (red glare).
- Whether a reflection is predicted to be operationally significant in practice or not.

Where no solar reflections are geometrically possible or where solar reflections are predicted to be significantly screened, no impact is predicted, and mitigation is not required.

Where solar reflections are of an intensity no greater than 'low potential for temporary after-image' (green glare) or occur outside of a pilot's primary field of view (50 degrees either side of the approach bearing), the impact significance is low, and mitigation is not recommended.

Glare with 'potential for a temporary after-image' (yellow glare) was formerly not permissible under the interim guidance provided by the Federal Aviation Administration in the USA<sup>12</sup> for on-airfield solar. Whilst this guidance was never formally applicable outside of the USA, it has been a common point of reference internationally. Pager Power recommends a pragmatic approach whereby instances of 'yellow' glare are evaluated in a technical and operational context. As per Pager Power's glint and glare guidance document<sup>13</sup>, where solar reflections are of an intensity

---

<sup>12</sup> This FAA guidance from 2013 has since been superseded by the FAA guidance in 2021 whereby airports are tasked with determining safety requirements themselves.

<sup>13</sup> [Pager Power Glint and Glare Guidance](#), Fourth Edition, September 2022.

no greater than 'low potential for temporary after-image' expert assessment of the following relevant factors is required to determine the impact significance<sup>14</sup>:

- The likely traffic volumes and level of safeguarding at the aerodrome – licensed aerodromes typically have higher traffic volumes and are formally safeguarded;
- The time of day at which glare is predicted and whether the aerodrome will be operational such that pilots can be on the approach at these times;
- The duration of any predicted glare – glare that occurs for low durations throughout the year is less likely to be experienced than glare that occurs for longer durations throughout the year;
- The location and size of the reflecting panel area relative to a pilot's primary field-of-view;
- The location of the source of glare relative to the position of the Sun at the times and dates in which solar reflections are geometrically possible – effects that coincide with direct Sunlight appear less prominent than those that do not;
- The level of predicted effect relative to existing sources of glare – a solar reflection is less noticeable by pilots when there are existing reflective surfaces in the surrounding environment.

Following consideration of these mitigating factors, where the solar reflection does not remain significant, a low impact is predicted, and mitigation is not recommended; however, consultation with the aerodrome is recommended to understand their position along with any feedback or comments regarding the development. Where the solar reflection remains significant, the impact significance is moderate, and mitigation is recommended.

Where solar reflections are of an intensity greater than 'potential for temporary after-image', the impact significance is high, and mitigation is required.

---

<sup>14</sup> This approach taken is reflective of the changes made in the 2021 FAA guidance; however, it should be noted that this guidance states that it is up to the airport to determine the safety requirements themselves. Therefore, an airport may not accept any yellow glare towards approach paths.

### 5.3 Road Receptors

The process for quantifying the impact significance concerning road safety is outlined in Appendix D. The key considerations for road users along major national, national, and regional roads are:

- Whether a reflection is predicted to be experienced in practice; and
- The location of the reflecting panel relative to a road user's direction of travel.

Where reflections are geometrically possible but expected to be screened, no impact is predicted, and mitigation is not required.

Where reflections originate from outside of a road user's primary horizontal field of view (50 degrees either side of the direction of travel), or the closest reflecting panel is over 1km from the road user, the impact significance is low, and mitigation is not recommended.

Where reflections are predicted to be experienced from inside of a road user's primary field of view, expert assessment of the following mitigating factors is required to determine the impact significance and mitigation requirement:

- Whether visibility is likely for elevated drivers (relevant to dual carriageways and motorways<sup>15</sup>);
- Whether the solar reflection originates from directly in front of a road user. Solar reflections that are directly in front of a road user are more hazardous;
- The separation distance to the reflecting panel area. Larger separation distances reduce the proportion of an observer's field of view that is affected by glare;
- The position of the Sun. Effects that coincide with direct sunlight appear less prominent than those that do not. The Sun is a far more significant source of light.

Following consideration of these mitigating factors, where the solar reflection does not remain significant, a low impact is predicted, and mitigation is not recommended. Where the solar reflection remains significant, the impact significance is moderate, and mitigation is recommended.

Where reflections originate from directly in front of a road user and there are no further mitigating factors, the impact significance is high, and mitigation is required.

---

<sup>15</sup> There is typically a higher density of elevated drivers (such as HGVs) along dual carriageways and motorways compared to other types of roads.

## 5.4 Dwelling Receptors

The process for quantifying the impact significance concerning residential amenity is outlined in Appendix D. The key considerations for residential dwellings are:

- Whether a reflection is predicted to be experienced in practice;
- The duration of the predicted effects, relative to thresholds of:
  - 3 months per year;
  - 60 minutes on any given day.

Where reflections are geometrically possible but expected to be screened, no impact is predicted, and mitigation is not required.

Where effects occur for less than 3 months per year and less than 60 minutes on any given day, or the closest reflecting panel is over 1km from the road user, the impact significance is low, and mitigation is not recommended.

Where reflections are predicted to be experienced for more than 3 months per year and/or for more than 60 minutes on any given day, expert assessment of the following mitigating factors is required to determine the impact significance and mitigation requirement:

- The separation distance to the reflecting panel area<sup>16</sup>. Larger separation distances reduce the proportion of an observer's field of view that is affected by glare;
- The position of the Sun. Effects that coincide with direct sunlight appear less prominent than those that do not. The Sun is a far more significant source of light;
- Whether solar reflections will be experienced from all storeys. The ground floor is typically considered the main living space and therefore has a greater significance with respect to residential amenity;
- Whether the dwelling appears to have windows facing the reflecting areas. An observer may need to look at an acute angle to observe the reflecting areas.

Following consideration of these mitigating factors, where the solar reflection does not remain significant, a low impact is predicted, and mitigation is not recommended. Where the solar reflection remains significant, the impact significance is moderate, and mitigation is recommended.

If there are no mitigating factors and the effects last for more than 3 months per year and for more than 60 minutes on any given day, the impact significance is high, and mitigation is required.

## 5.5 Report Summary

The receptors to be assessed within the glint and glare assessment to be submitted as part of the DCO application include aviation receptors associated with Cambridge Airport and Duxford Aerodrome, 4.5km of the A11, 2.7km of the B1052, 6.1km of Balsham /Cambridge Road and 111 dwelling receptors.

---

<sup>16</sup> Which is often greater than the nearest panel boundary, because not all areas of the site cause specular reflections towards particular receptor locations.

## APPENDIX A – OVERVIEW OF GLINT AND GLARE GUIDANCE

### Overview

This section presents details regarding the relevant guidance and studies with respect to the considerations and effects of solar reflections from solar panels, known as 'Glint and Glare'.

This is not a comprehensive review of the data sources, rather it is intended to give an overview of the important parameters and considerations that have informed this assessment.

### UK Planning Policy

#### Renewable and Low Carbon Energy

The National Planning Policy Framework under the planning practice guidance for Renewable and Low Carbon Energy<sup>17</sup> (specifically regarding the consideration of solar farms, paragraph 013) states:

'What are the particular planning considerations that relate to large scale ground-mounted solar photovoltaic Farms?

The deployment of large-scale solar farms can have a negative impact on the rural environment, particularly in undulating landscapes. However, the visual impact of a well-planned and well-screened solar farm can be properly addressed within the landscape if planned sensitively.

Particular factors a local planning authority will need to consider include:

...

- the proposal's visual impact, the effect on landscape of glint and glare (see guidance on landscape assessment) and on **neighbouring uses and aircraft safety**;
- the extent to which there may be additional impacts if solar arrays follow the daily movement of the sun;

...

The approach to assessing cumulative landscape and visual impact of large scale solar farms is likely to be the same as assessing the impact of wind turbines. However, in the case of ground-mounted solar panels it should be noted that with effective screening and appropriate land topography the area of a zone of visual influence could be zero.'

---

<sup>17</sup> Renewable and low carbon energy, Ministry of Housing, Communities & Local Government, date: 18 June 2015, accessed on: 01/11/2021

## National Policy Statement for Renewable Energy Infrastructure

The National Policy Statement for Renewable Energy Infrastructure (EN-3)<sup>18</sup> sets out the primary policy for decisions by the Secretary of State for nationally significant renewable energy infrastructure. Sections 2.10.102-106 state:

*'2.10.102 Solar panels are specifically designed to absorb, not reflect, irradiation.<sup>19</sup> However, solar panels may reflect the sun's rays at certain angles, causing glint and glare. Glint is defined as a momentary flash of light that may be produced as a direct reflection of the sun in the solar panel. Glare is a continuous source of excessive brightness experienced by a stationary observer located in the path of reflected sunlight from the face of the panel. The effect occurs when the solar panel is stationed between or at an angle of the sun and the receptor.'*

*2.10.103 Applicants should map receptors to qualitatively identify potential glint and glare issues and determine if a glint and glare assessment is necessary as part of the application.*

*2.10.104 When a quantitative glint and glare assessment is necessary, applicants are expected to consider the geometric possibility of glint and glare affecting nearby receptors and provide an assessment of potential impact and impairment based on the angle and duration of incidence and the intensity of the reflection.*

*2.10.105 The extent of reflectivity analysis required to assess potential impacts will depend on the specific project site and design. This may need to account for 'tracking' panels if they are proposed as these may cause differential diurnal and/or seasonal impacts.*

*2.10.106 When a glint and glare assessment is undertaken, the potential for solar PV panels, frames and supports to have a combined reflective quality may need to be assessed, although the glint and glare of the frames and supports is likely to be significantly less than the panels.'*

The EN-3 does not state which receptors should be considered as part of a quantitative glint and glare assessment. Based on Pager Power's extensive project experience, typical receptors include residential dwellings, road users, aviation infrastructure, and railway infrastructure.

Sections 2.10.134-136 state:

*'2.10.134 Applicants should consider using, and in some cases the Secretary of State may require, solar panels to comprise of (or be covered with) anti-glare/anti-reflective coating with a specified angle of maximum reflection attenuation for the lifetime of the permission.*

*2.10.135 Applicants may consider using screening between potentially affected receptors and the reflecting panels to mitigate the effects.*

*2.10.136 Applicants may consider adjusting the azimuth alignment of or changing the elevation tilt angle of a solar panel, within the economically viable range, to alter the angle of incidence.*

---

<sup>18</sup> National Policy Statement for Renewable Energy Infrastructure (EN-3), Department for Energy Security & Net Zero, date: November 2023, accessed on: 21/12/2023.

<sup>19</sup> 'Most commercially available solar panels are designed with anti-reflective glass or are produced with anti-reflective coating and have a reflective capacity that is generally equal to or less hazardous than other objects typically found in the outdoor environment, such as bodies of water or glass buildings.'



*In practice this is unlikely to remove the potential impact altogether but in marginal cases may contribute to a mitigation strategy.'*

The mitigation strategies listed within the EN-3 are relevant strategies that are frequently utilised to eliminate or reduce glint and glare effects towards surrounding observers. The most common form of mitigation is the implementation of screening along the site boundary.

Sections 2.10.158-159 state:

*2.10.158 Solar PV panels are designed to absorb, not reflect, irradiation. However, the Secretary of State should assess the potential impact of glint and glare on nearby homes, motorists, public rights of way, and aviation infrastructure (including aircraft departure and arrival flight paths).*

*2.10.159 Whilst there is some evidence that glint and glare from solar farms can be experienced by pilots and air traffic controllers in certain conditions, there is no evidence that glint and glare from solar farms results in significant impairment on aircraft safety. Therefore, unless a significant impairment can be demonstrated, the Secretary of State is unlikely to give any more than limited weight to claims of aviation interference because of glint and glare from solar farms.*

The EN-3 goes some way in acknowledging that the issue is more complex than presented in the early draft issues; though, this is still unlikely to be welcomed by aviation stakeholders, who will still request a glint and glare assessment on the basis that glare may lead to a potentially significant impact upon aviation safety.

Finally, the EN-3 relates solely to nationally significant renewable energy infrastructure and therefore does not apply to all planning applications for solar farms.

### **Assessment Process – Ground-Based Receptors**

No process for determining and contextualising the effects of glint and glare has been determined when assessing the impact of solar reflections upon surrounding roads and dwellings. Therefore, the Pager Power approach is to determine whether a reflection from the proposed solar development is geometrically possible and then to compare the results against the relevant guidance/studies to determine whether the reflection is significant.

The Pager Power approach has been informed by the policy presented above, current studies (presented in Appendix B) and stakeholder consultation. Further information can be found in Pager Power's Glint and Glare Guidance document<sup>20</sup> which was produced due to the absence of existing guidance and a specific standardised assessment methodology.

---

<sup>20</sup> Solar Photovoltaic Development Glint and Glare Guidance, Fourth Edition, March 2022. Pager Power.

## Aviation Assessment Guidance

The UK Civil Aviation Authority (CAA) issued interim guidance relating to Solar Photovoltaic Systems (SPV) on 17 December 2010 and was subject to a CAA information alert 2010/53. The formal policy was cancelled on September 7<sup>th</sup>, 2012<sup>21</sup> however the advice is still applicable<sup>22</sup> until a formal policy is developed. The relevant aviation guidance from the CAA is presented in the section below.

### CAA Interim Guidance

This interim guidance makes the following recommendations (p.2-3):

*'8. It is recommended that, as part of a planning application, the SPV developer provide safety assurance documentation (including risk assessment) regarding the full potential impact of the SPV installation on aviation interests.*

*9. Guidance on safeguarding procedures at CAA licensed aerodromes is published within CAP 738 Safeguarding of Aerodromes and advice for unlicensed aerodromes is contained within CAP 793 Safe Operating Practices at Unlicensed Aerodromes.*

*10. Where Schemes in the vicinity of aerodromes require an application for planning permission the relevant LPA normally consults aerodrome operators or NATS when aeronautical interests might be affected. This consultation procedure is a statutory obligation in the case of certain major airports, and may include military establishments and certain air traffic surveillance technical sites. These arrangements are explained in Department for Transport Circular 1/2003 and for Scotland, Scottish Government Circular 2/2003.*

*11. In the event of SPV developments proposed under the Electricity Act, the relevant government department should routinely consult with the CAA. There is therefore no requirement for the CAA to be separately consulted for such proposed SPV installations or developments.*

*12. If an installation of SPV systems is planned on-aerodrome (i.e. within its licensed boundary) then it is recommended that data on the reflectivity of the solar panel material should be included in any assessment before installation approval can be granted. Although approval for installation is the responsibility of the ALH<sup>23</sup>, as part of a condition of a CAA Aerodrome Licence, the ALH is required to obtain prior consent from CAA Aerodrome Standards Department before any work is begun or approval to the developer or LPA is granted, in accordance with the procedures set out in CAP 791 Procedures for Changes to Aerodrome Infrastructure.*

*13. During the installation and associated construction of SPV systems there may also be a need to liaise with nearby aerodromes if cranes are to be used; CAA notification and permission is not required.*

*14. The CAA aims to replace this informal guidance with formal policy in due course and reserves the right to cancel, amend or alter the guidance provided in this document at its discretion upon receipt of new information.*

---

<sup>21</sup> Archived at Pager Power

<sup>22</sup> Reference email from the CAA dated 19/05/2014.

<sup>23</sup> Aerodrome Licence Holder.

15. Further guidance may be obtained from CAA's Aerodrome Standards Department via [aerodromes@caa.co.uk](mailto:aerodromes@caa.co.uk).'

### **FAA Guidance**

The most comprehensive guidelines available for the assessment of solar developments near aerodromes has been produced by the United States Federal Aviation Administration (FAA). The first guidelines were produced initially in November 2010 and updated in 2013. A final policy was released in 2021, which superseded the interim guidance.

The 2010 document is entitled 'Technical Guidance for Evaluating Selected Solar Technologies on Airports'<sup>24</sup>, the 2013 update is entitled 'Interim Policy, FAA Review of Solar Energy System Projects on Federally Obligated Airports'<sup>25</sup>, and the 2021 final policy is entitled 'Federal Aviation Administration Policy: Review of Solar Energy System Projects on Federally-Obligated Airports'<sup>26</sup>.

Key excerpts from the final policy are presented below:

*Initially, FAA believed that solar energy systems could introduce a novel glint and glare effect to pilots on final approach. FAA has subsequently concluded that in most cases, the glint and glare from solar energy systems to pilots on final approach is similar to glint and glare pilots routinely experience from water bodies, glass-façade buildings, parking lots, and similar features. However, FAA has continued to receive reports of potential glint and glare from on-airport solar energy systems on personnel working in ATCT cabs. Therefore, FAA has determined the scope of agency policy should be focused on the impact of on-airport solar energy systems to federally-obligated towered airports, specifically the airport's ATCT cab.*

*The policy in this document updates and replaces the previous policy by encouraging airport sponsors to conduct an ocular analysis of potential impacts to ATCT cabs prior to submittal of a Notice of Proposed Construction or Alteration Form 7460-1 (hereinafter Form 7460-1). Airport sponsors are no longer required to submit the results of an ocular analysis to FAA. Instead, to demonstrate compliance with 14 CFR 77.5(c), FAA will rely on the submittal of Form 7460-1 in which the sponsor confirms that it has analyzed the potential for glint and glare and determined there is no potential for ocular impact to the airport's ATCT cab. This process will enable FAA to evaluate the solar energy system project, with assurance that the system will not impact the ATCT cab.*

*FAA encourages airport sponsors of federally-obligated towered airports to conduct a sufficient analysis to support their assertion that a proposed solar energy system will not result in ocular impacts. There are several tools available on the open market to airport sponsors that can analyze potential glint and glare to an ATCT cab. For proposed systems that will clearly not impact ATCT cabs (e.g., on-airport solar energy systems that are blocked from the ATCT cab's view by another structure), the use of such tools may not be necessary to support the assertion that a proposed solar energy system will not result in ocular impacts.*

---

<sup>24</sup> Archived at Pager Power

<sup>25</sup> Interim Policy, FAA Review of Solar Energy System Projects on Federally Obligated Airports, Department of Transportation, Federal Aviation Administration (FAA), date: 10/2013, accessed on: 08/12/2021.

<sup>26</sup> Federal Aviation Administration Policy: Review of Solar Energy System Projects on Federally-Obligated Airports, Federal Aviation Administration, date: May 2021, accessed on: 08/12/2021.

The excerpt above states where a solar PV development is to be located on a federally obligated aerodrome with an ATC Tower, it will require a glint and glare assessment to accompany its application. It states that pilots on approach are no longer a specific assessment requirement due to effects from solar energy systems being similar to glint and glare pilots routinely experience from water bodies, glass-façade buildings, parking lots, and similar features. Ultimately it comes down to the specific aerodrome to ensure it is adequately safeguarded, and it is on this basis that glint and glare assessments are routinely still requested.

The policy also states that several different tools and methodologies can be used to assess the impacts of glint and glare, which was previously required to be undertaken by the Solar Glare Hazard Analysis Tool (SGHAT) using the Sandia National Laboratories methodology.

In 2018, the FAA released the latest version (Version 1.1) of the '*Technical Guidance for Evaluating Selected Solar Technologies on Airports*'<sup>27</sup>. Whilst the 2021 final policy also supersedes this guidance, many of the points are still relevant because aerodromes are still safeguarding against glint and glare irrespective of the FAA guidance. The key points are presented below for reference:

- *Reflectivity refers to light that is reflected off surfaces. The potential effects of reflectivity are glint (a momentary flash of bright light) and glare (a continuous source of bright light). These two effects are referred to hereinafter as "glare," which can cause a brief loss of vision, also known as flash blindness*<sup>28</sup>.
- *The amount of light reflected off a solar panel surface depends on the amount of sunlight hitting the surface, its surface reflectivity, geographic location, time of year, cloud cover, and solar panel orientation.*
- *As illustrated on Figure 16<sup>29</sup>, flat, smooth surfaces reflect a more concentrated amount of sunlight back to the receiver, which is referred to as specular reflection. The more a surface is polished, the more it shines. Rough or uneven surfaces reflect light in a diffused or scattered manner and, therefore, the light will not be received as bright.*
- *Because the FAA has no specific standards for airport solar facilities and potential glare, the type of glare analysis may vary. Depending on site specifics (e.g., existing land uses, location and size of the project) an acceptable evaluation could involve one or more of the following levels of assessment:*
  - *A qualitative analysis of potential impact in consultation with the Control Tower, pilots and airport officials;*
  - *A demonstration field test with solar panels at the proposed site in coordination with FAA Tower personnel;*
  - *A geometric analysis to determine days and times when an impact is predicted.*

---

<sup>27</sup> Technical Guidance for Evaluating Selected Solar Technologies on Airports, Federal Aviation Administration (FAA), date: 04/2018, accessed on: 08/12/2021.

<sup>28</sup> Flash Blindness, as described in the FAA guidelines, can be described as a temporary visual interference effect that persists after the source of illumination has ceased. This occurs from many reflective materials in the ambient environment.

<sup>29</sup> First figure in Appendix B.

- The extent of reflectivity analysis required to assess potential impacts will depend on the specific project site and system design.
- **1. Assessing Baseline Reflectivity Conditions** – Reflection in the form of glare is present in current aviation operations. The existing sources of glare come from glass windows, auto surface parking, rooftops, and water bodies. At airports, existing reflecting surfaces may include hangar roofs, surface parking, and glassy office buildings. To minimize unexpected glare, windows of air traffic control towers and airplane cockpits are coated with anti-reflective glazing. Operators also wear polarized eye wear. Potential glare from solar panels should be viewed in this context. Any airport considering a solar PV project should first review existing sources of glare at the airport and the effectiveness of measures used to mitigate that glare.
- **2. Tests in the Field** – Potential glare from solar panels can easily be viewed at the airport through a field test. A few airports have coordinated these tests with FAA Air Traffic Controllers to assess the significance of glare impacts. To conduct such a test, a sponsor can take a solar panel out to proposed location of the solar project, and tilt the panel in different directions to evaluate the potential for glare onto the air traffic control tower. For the two known cases where a field test was conducted, tower personnel determined the glare was not significant. If there is a significant glare impact, the project can be modified by ensuring panels are not directed in that direction.
- **3. Geometric Analysis** – Geometric studies are the most technical approach for reflectivity issues. They are conducted when glare is difficult to assess through other methods. Studies of glare can employ geometry and the known path of the sun to predict when sunlight will reflect off of a fixed surface (like a solar panel) and contact a fixed receptor (e.g., control tower). At any given site, the sun moves across the sky every day and its path in the sky changes throughout year. This in turn alters the destination of the resultant reflections since the angle of reflection for the solar panels will be the same as the angle at which the sun hits the panels. The larger the reflective surface, the greater the likelihood of glare impacts.
- Facilities placed in remote locations, like the desert, will be far from receptors and therefore potential impacts are limited to passing aircraft. Because the intensity of the light reflected from the solar panel decreases with increasing distance, an appropriate question is how far you need to be from a solar reflected surface to avoid flash blindness. It is known that this distance is directly proportional to the size of the array in question<sup>30</sup> but still requires further research to definitively answer.
- **Experiences of Existing Airport Solar Projects** – Solar installations are presently operating at a number of airports, including megawatt-sized solar facilities covering multiple acres. Air traffic control towers have expressed concern about glint and glare from a small number of solar installations. These were often instances when solar installations were sited between the tower and airfield, or for installations with inadequate or no reflectivity analysis.

---

<sup>30</sup> Ho, Clifford, Cheryl Ghanbari, and Richard Diver. 2009. Hazard Analysis of Glint and Glare From Concentrating Solar Power Plants. SolarPACES 2009, Berlin Germany. Sandia National Laboratories.

*Adequate reflectivity analysis and alternative siting addressed initial issues at those installations.*

### **Air Navigation Order (ANO) 2016**

In some instances, an aviation stakeholder can refer to the ANO 2016<sup>31</sup> with regard to safeguarding. Key points from the document are presented below.

#### ***Lights liable to endanger***

224. (1) A person must not exhibit in the United Kingdom any light which—

(a) by reason of its glare is liable to endanger aircraft taking off from or landing at an aerodrome; or  
(b) by reason of its liability to be mistaken for an aeronautical ground light is liable to endanger aircraft.

(2) If any light which appears to the CAA to be a light described in paragraph (1) is exhibited, the CAA may direct the person who is the occupier of the place where the light is exhibited or who has charge of the light, to take such steps within a reasonable time as are specified in the direction—

(a) to extinguish or screen the light; and

(b) to prevent in the future the exhibition of any other light which may similarly endanger aircraft.

(3) The direction may be served either personally or by post, or by affixing it in some conspicuous place near to the light to which it relates.

(4) In the case of a light which is or may be visible from any waters within the area of a general lighthouse authority, the power of the CAA under this article must not be exercised except with the consent of that authority.

#### ***Lights which dazzle or distract***

225. A person must not in the United Kingdom direct or shine any light at any aircraft in flight so as to dazzle or distract the pilot of the aircraft.'

The document states that no 'light', 'dazzle' or 'glare' should be produced which will create a detrimental impact upon aircraft safety.

#### ***Endangering safety of an aircraft***

240. A person must not recklessly or negligently act in a manner likely to endanger an aircraft, or any person in an aircraft.

---

<sup>31</sup> The Air Navigation Order 2016. [online] Available at:  
<<https://www.legislation.gov.uk/uksi/2016/765/contents/made>> [Accessed 4 February 2022].

***Endangering safety of any person or property***

241. *A person must not recklessly or negligently cause or permit an aircraft to endanger any person or property.*

**Civil Aviation Authority consolidation of UK Regulation 139/2014**

The Civil Aviation Authority (CAA) published a consolidating document<sup>32</sup> of UK regulations, (Implementing Rules, Acceptable Means of Compliance and Guidance Material), in 2023. A summary of material relevant to aerodrome safeguarding is presented below:

(a) The aerodrome operator should have procedures to monitor the changes in the obstacle environment, marking and lighting, and in human activities or land use on the aerodrome and the areas around the aerodrome, as defined in coordination with the CAA. The scope, limits, tasks and responsibilities for the monitoring should be defined in coordination with the relevant air traffic services providers, and with the CAA and other relevant authorities.

(b) The limits of the aerodrome surroundings that should be monitored by the aerodrome operator are defined in coordination with the CAA and should include the areas that can be visually monitored during the inspections of the manoeuvring area.

(c) The aerodrome operator should have procedures to mitigate the risks associated with changes on the aerodrome and its surroundings identified with the monitoring procedures. The scope, limits, tasks, and responsibilities for the mitigation of risks associated to obstacles or hazards outside the perimeter fence of the aerodrome should be defined in coordination with the relevant air traffic services providers, and with the CAA and other relevant authorities.

(d) The risks caused by human activities and land use which should be assessed and mitigated should include:

1. obstacles and the possibility of induced turbulence;
2. the use of hazardous, confusing, and misleading lights;
3. the dazzling caused by large and highly reflective surfaces;
4. sources of non-visible radiation, or the presence of moving, or fixed objects which may interfere with, or adversely affect, the performance of aeronautical communications, navigation and surveillance systems; and
5. non-aeronautical ground light near an aerodrome which may endanger the safety of aircraft and which should be extinguished, screened, or otherwise modified so as to eliminate the source of danger.

---

<sup>32</sup> <https://regulatorylibrary.caa.co.uk/139-2014-pdf/PDF.pdf>

## APPENDIX B – OVERVIEW OF GLINT AND GLARE STUDIES

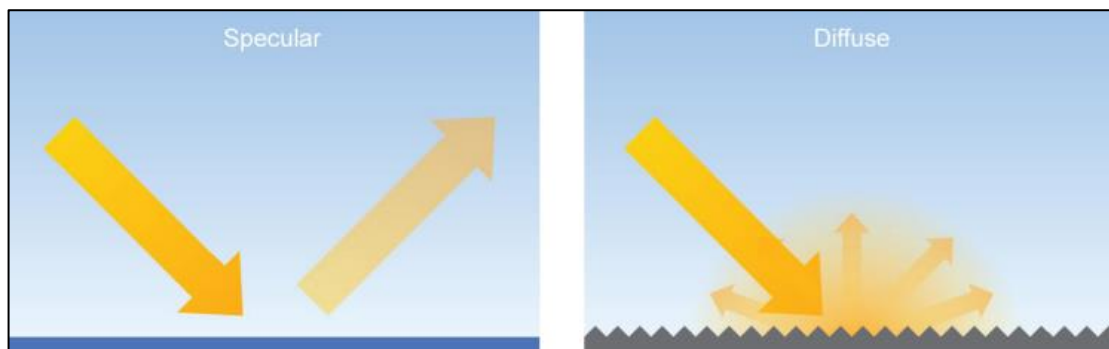
### Overview

Studies have been undertaken assessing the type and intensity of solar reflections from various surfaces including solar panels and glass. An overview of these studies is presented below.

The guidelines presented are related to aviation safety. The results are applicable for the purpose of this analysis.

### Reflection Type from Solar Panels

Based on the surface conditions reflections from light can be specular and diffuse. A specular reflection has a reflection characteristic similar to that of a mirror; a diffuse reflection will reflect the incoming light and scatter it in many directions. The figure below, taken from the FAA guidance<sup>33</sup>, illustrates the difference between the two types of reflections. Because solar panels are flat and have a smooth surface most of the light reflected is specular, which means that incident light from a specific direction is reradiated in a specific direction.



*Specular and diffuse reflections*

---

<sup>33</sup> [Technical Guidance for Evaluating Selected Solar Technologies on Airports](#), Federal Aviation Administration (FAA), date: 04/2018, accessed on: 08/12/2021.

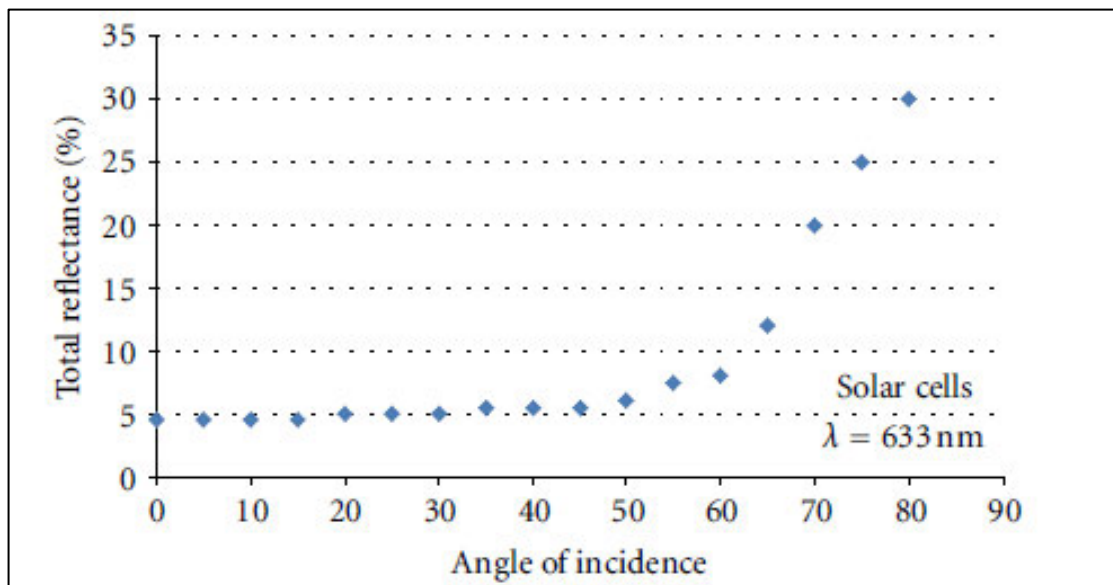


## Solar Reflection Studies

An overview of content from identified solar panel reflectivity studies is presented in the subsections below.

### Evan Riley and Scott Olson, “A Study of the Hazardous Glare Potential to Aviators from Utility-Scale Flat-Plate Photovoltaic Systems”

Evan Riley and Scott Olson published in 2011 their study titled: *A Study of the Hazardous Glare Potential to Aviators from Utility-Scale Flat-Plate Photovoltaic Systems*<sup>34</sup>. They researched the potential glare that a pilot could experience from a 25-degree fixed tilt PV system located outside of Las Vegas, Nevada. The theoretical glare was estimated using published ocular safety metrics which quantify the potential for a postflash glare after-image. This was then compared to the postflash glare after-image caused by smooth water. The study demonstrated that the reflectance of the solar cell varied with angle of incidence, with maximum values occurring at angles close to 90 degrees. The reflectance values varied from approximately 5% to 30%. This is shown on the figure below.



Total reflectance % when compared to angle of incidence

The conclusions of the research study were:

- The potential for hazardous glare from flat-plate PV systems is similar to that of smooth water;
- Portland white cement concrete (which is a common concrete for runways), snow, and structural glass all have a reflectivity greater than water and flat plate PV modules.

<sup>34</sup> Evan Riley and Scott Olson, “A Study of the Hazardous Glare Potential to Aviators from Utility-Scale Flat-Plate Photovoltaic Systems,” *ISRN Renewable Energy*, vol. 2011, Article ID 651857, 6 pages, 2011. doi:10.5402/2011/651857

**FAA Guidance - “Technical Guidance for Evaluating Selected Solar Technologies on Airports”<sup>35</sup>**

The 2018 FAA Guidance included a diagram which illustrates the relative reflectance of solar panels compared to other surfaces. The figure shows the relative reflectance of solar panels compared to other surfaces. Surfaces in this figure produce reflections which are specular and diffuse. A specular reflection (those made by most solar panels) has a reflection characteristic similar to that of a mirror. A diffuse reflection will reflect the incoming light and scatter it in many directions. A table of reflectivity values, sourced from the figure within the FAA guidance, is presented below.

Surface	Approximate Percentage of Light Reflected <sup>36</sup>
Snow	80
White Concrete	77
Bare Aluminium	74
Vegetation	50
Bare Soil	30
Wood Shingle	17
Water	5
Solar Panels	5
Black Asphalt	2

*Relative reflectivity of various surfaces*

Note that the data above does not appear to consider the reflection type (specular or diffuse).

An important comparison in this table is the reflectivity compared to water which will produce a reflection of very similar intensity when compared to that from a solar panel. The study by Riley and Olsen study (2011) also concludes that still water has a very similar reflectivity to solar panels.

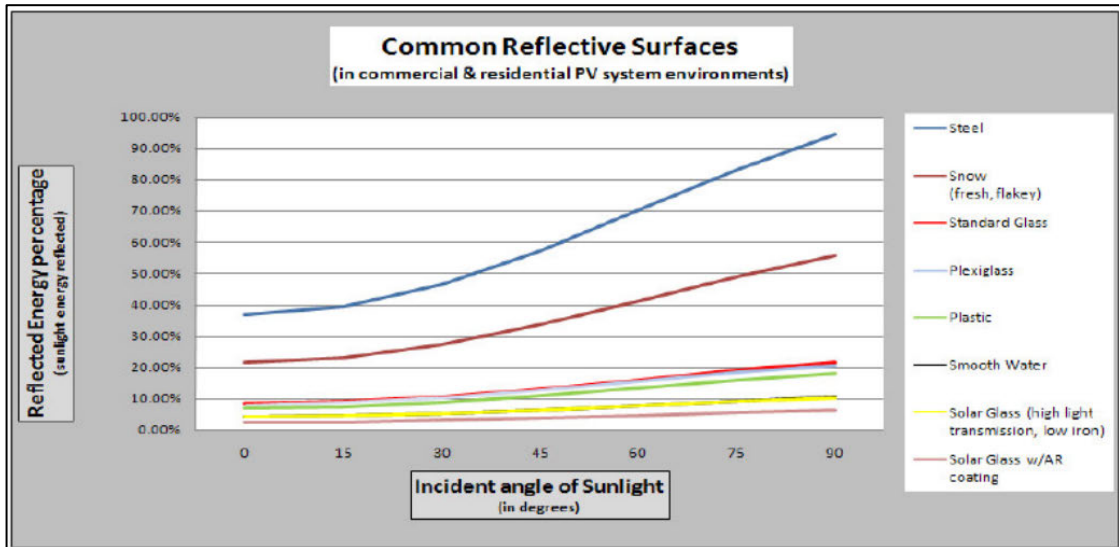
<sup>35</sup> [Technical Guidance for Evaluating Selected Solar Technologies on Airports](#), Federal Aviation Administration (FAA), date: 04/2018, accessed on: 08/12/2021.

<sup>36</sup> Extrapolated data, baseline of 1,000 W/m<sup>2</sup> for incoming sunlight.

**SunPower Technical Notification (2009)**

SunPower published a technical notification<sup>37</sup> to 'increase awareness concerning the possible glare and reflectance impact of PV Systems on their surrounding environment'.

The figure presented below shows the relative reflectivity of solar panels compared to other natural and manmade materials including smooth water, standard glass and steel.



Common reflective surfaces

The results, similarly to those from Riley and Olsen study (2011) and the FAA (2010), show that solar panels produce a reflection that is less intense than those of 'standard glass and other common reflective surfaces'.

With respect to aviation and solar reflections observed from the air, SunPower has developed several large installations near airports or on Air Force bases. It is stated that these developments have all passed FAA or Air Force standards with all developments considered "No Hazard to Air Navigation". The note suggests that developers discuss any possible concerns with stakeholders near proposed solar farms.

<sup>37</sup> Source: Technical Support, 2009. SunPower Technical Notification – Solar Module Glare and Reflectance.

## APPENDIX C – OVERVIEW OF SUN MOVEMENTS AND RELATIVE REFLECTIONS

The Sun's position in the sky can be accurately described by its azimuth and elevation. Azimuth is a direction relative to true north (horizontal angle i.e. from left to right) and elevation describes the Sun's angle relative to the horizon (vertical angle i.e. up and down).

The Sun's position can be accurately calculated for a specific location. The following data being used for the calculation:

- Time;
- Date;
- Latitude;
- Longitude.

The following is true at the location of the solar development:

- The Sun is at its highest around midday and is to the south at this time;
- The Sun rises highest on 21 June (longest day);
- On 21 December, the maximum elevation reached by the Sun is at its lowest (shortest day).

The combination of the Sun's azimuth angle and vertical elevation will affect the direction and angle of the reflection from a reflector.

## APPENDIX D – GLINT AND GLARE IMPACT SIGNIFICANCE

### Overview

The significance of glint and glare will vary for different receptors. The following section presents a general overview of the significance criteria with respect to experiencing a solar reflection.

### Impact Significance Definition

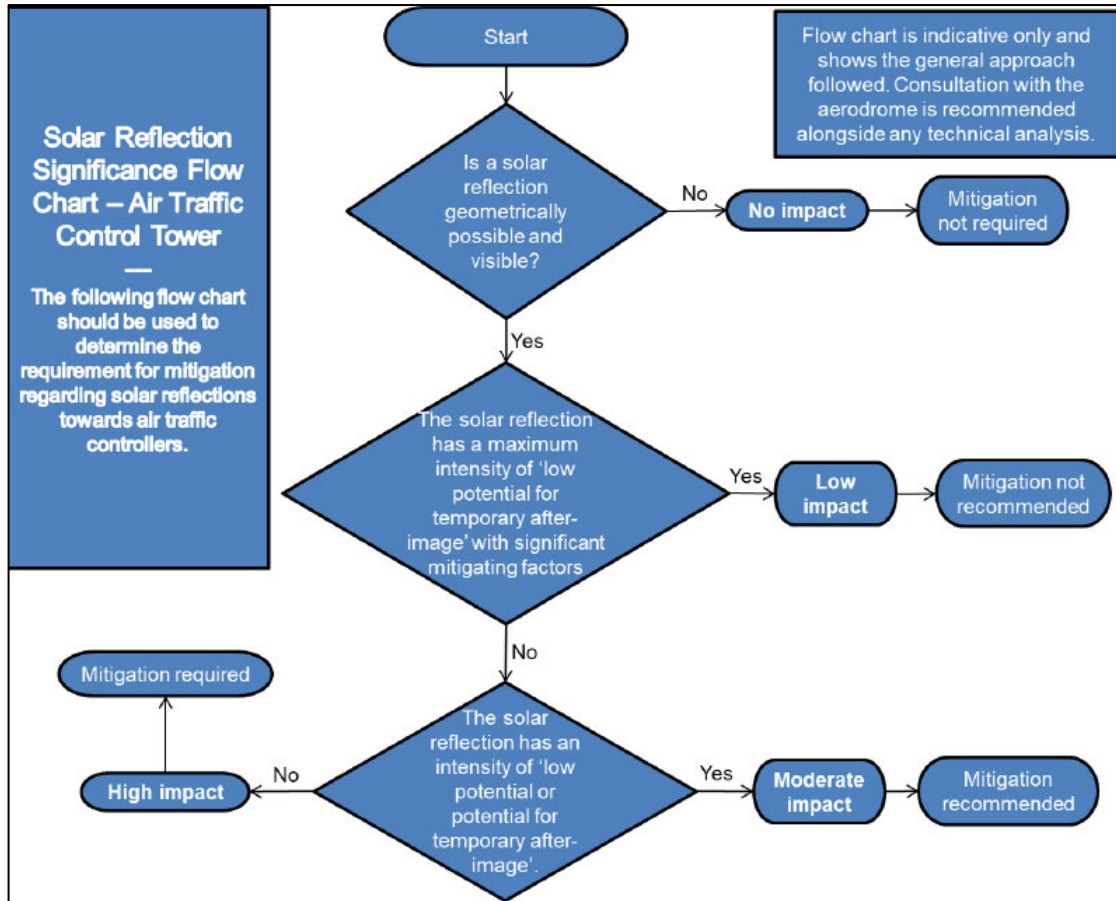
The table below presents the recommended definition of ‘impact significance’ in glint and glare terms and the requirement for mitigation under each.

Impact Significance	Definition	Mitigation
No Impact	A solar reflection is not geometrically possible or will not be visible from the assessed receptor.	No mitigation required.
Low	A solar reflection is geometrically possible however any impact is considered to be small such that mitigation is not required e.g. intervening screening will limit the view of the reflecting solar panels significantly.	No mitigation recommended.
Moderate	A solar reflection is geometrically possible and visible however it occurs under conditions that do not represent a worst-case given individual receptor criteria.	Mitigation recommended.
High	A solar reflection is geometrically possible and visible under worst-case conditions that will produce a significant impact given individual receptor criteria	Mitigation will be required if the development is to proceed.

*Impact significance definition*

### Impact Significance Determination for ATC Tower

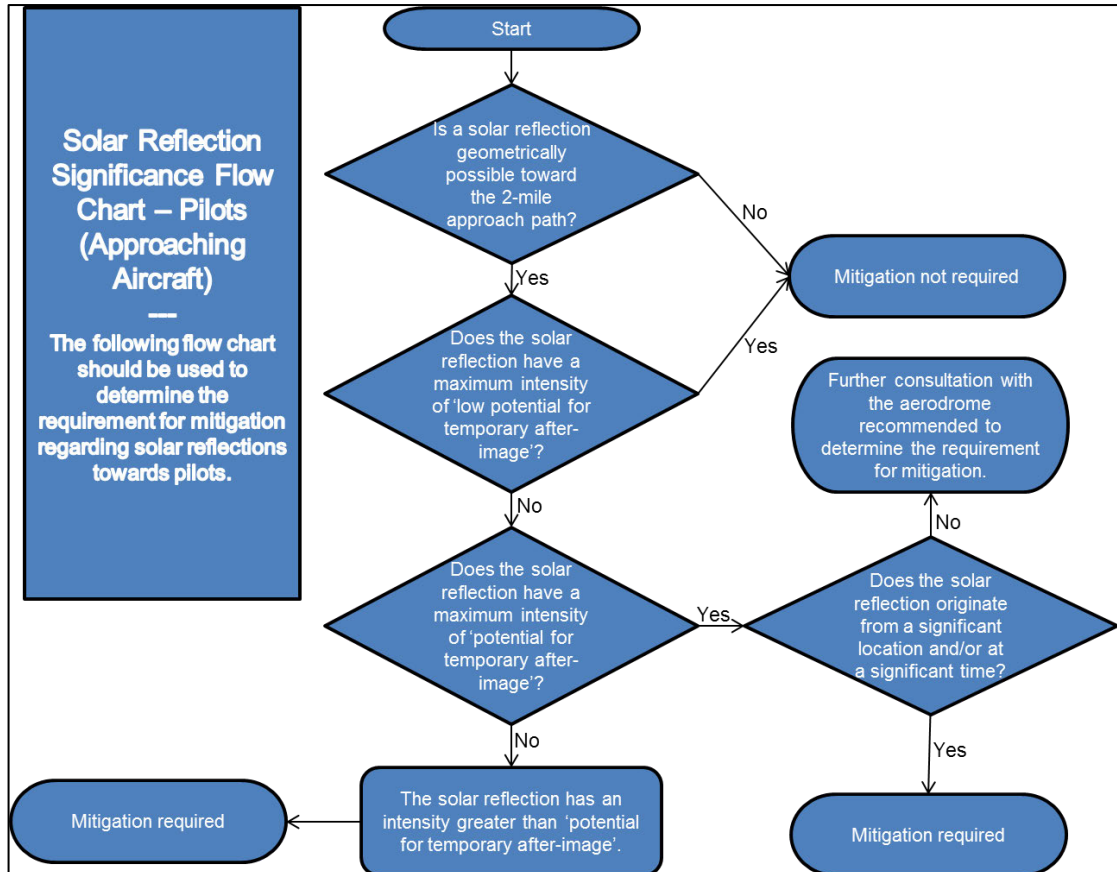
The flow chart presented below has been followed when determining the impact significance and mitigation requirement for ATC Tower receptors.



ATC Tower receptor mitigation requirement flow chart

### Impact Significance Determination for Approaching Aircraft

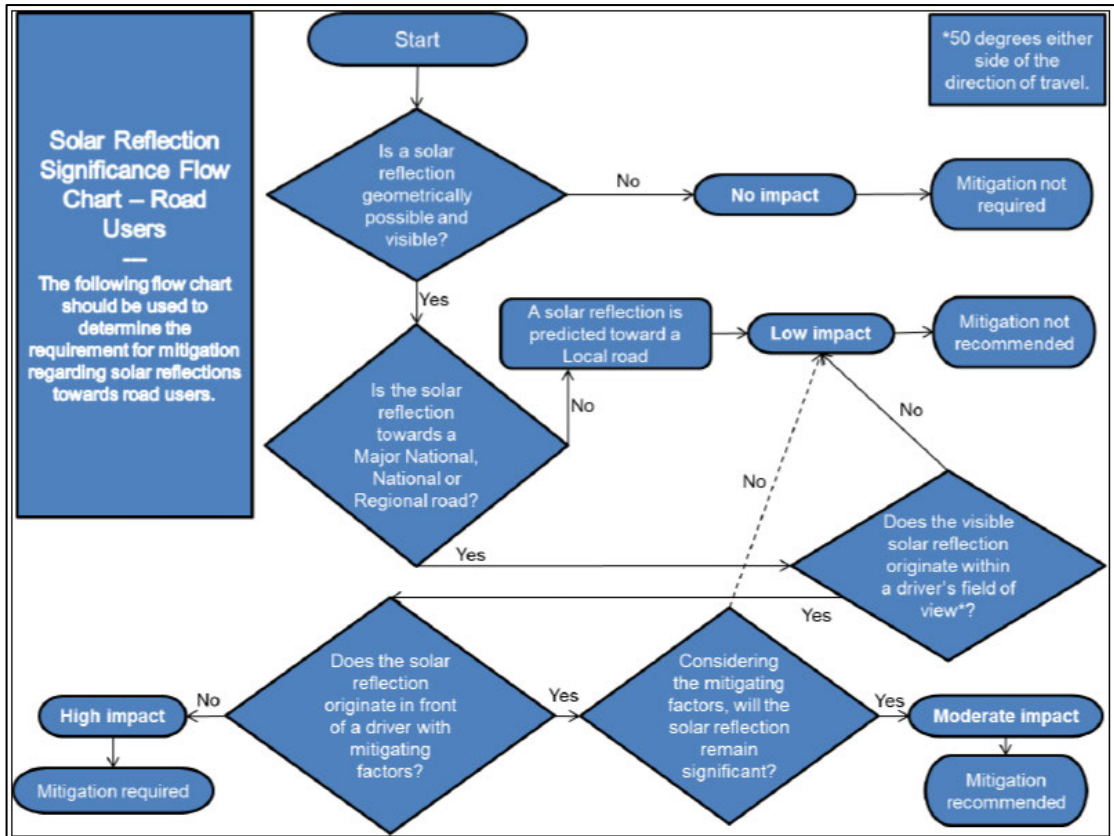
The flow chart presented below has been followed when determining the mitigation requirement for approaching aircraft.



Approaching aircraft receptor mitigation requirement flow chart

## Impact Significance Determination for Road Receptors

The flow chart presented below has been followed when determining the mitigation requirement for road receptors.

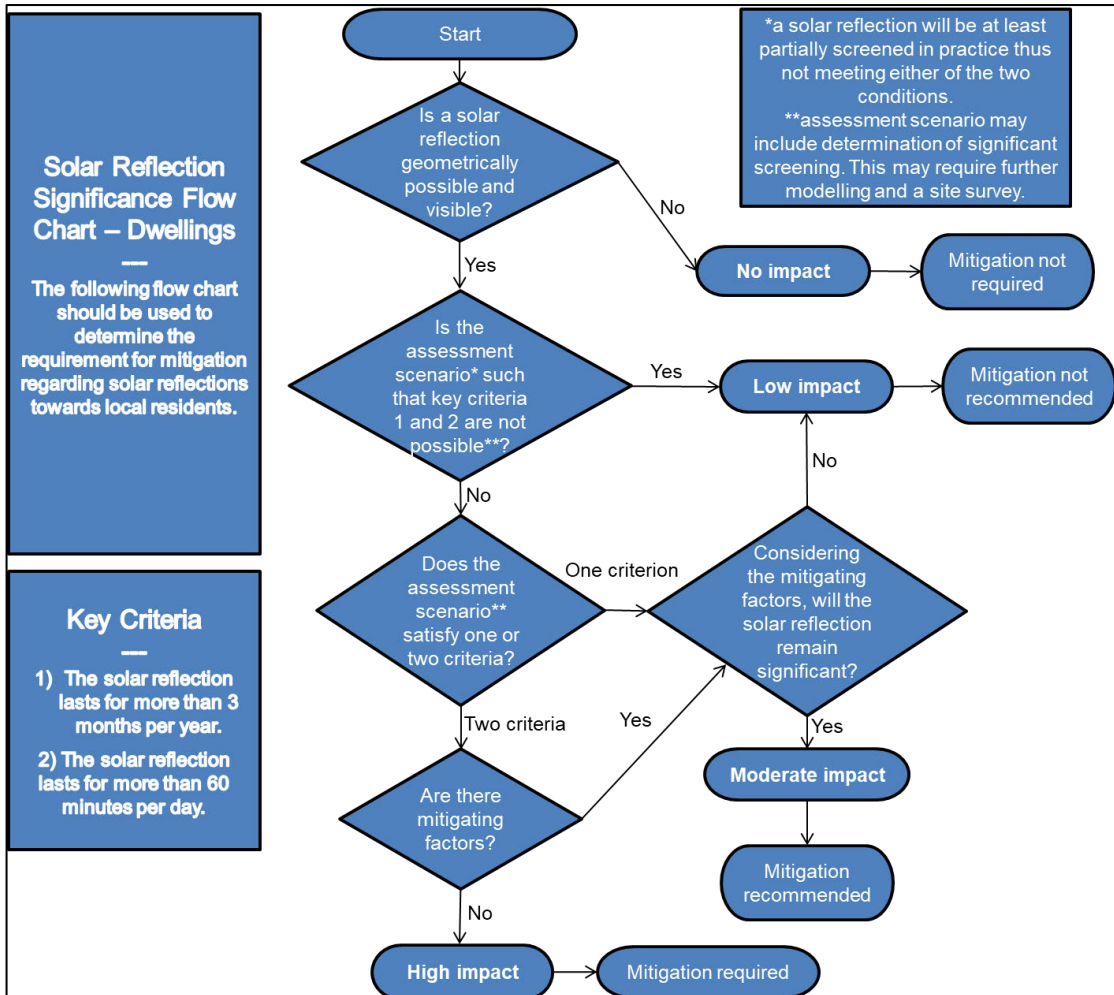


Road receptor mitigation requirement flow chart



## Impact Significance Determination for Dwelling Receptors

The flow chart presented below has been followed when determining the mitigation requirement for dwelling receptors.



Dwelling receptor mitigation requirement flow chart

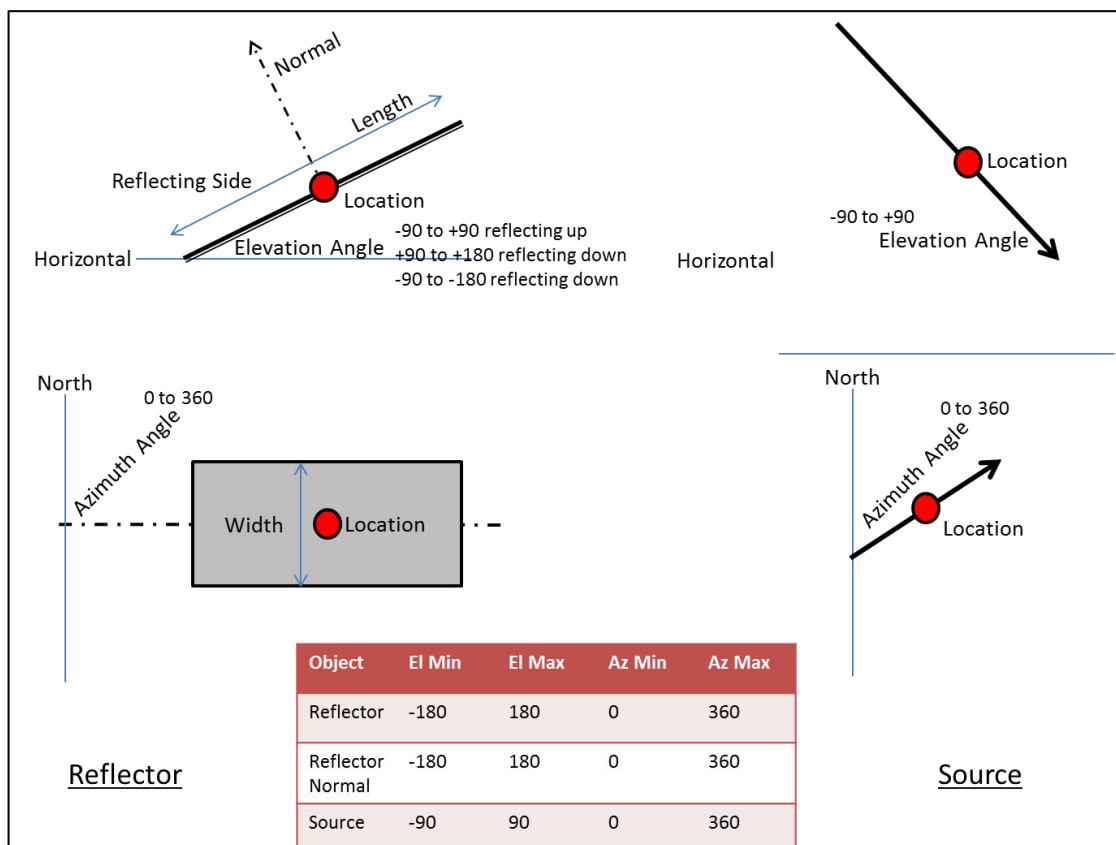
## APPENDIX E – REFLECTION CALCULATIONS METHODOLOGY

### Pager Power Methodology

The calculations are three dimensional and complex, accounting for:

- The Earth’s orbit around the Sun;
- The Earth’s rotation;
- The Earth’s orientation;
- The reflector’s location;
- The reflector’s 3D Orientation.

Reflections from a flat reflector are calculated by considering the normal which is an imaginary line that is perpendicular to the reflective surface and originates from it. The diagram below may be used to aid understanding of the reflection calculation process.



Reflection calculation process

The following process is used to determine the 3D Azimuth and Elevation of a reflection:

- Use the Latitude and Longitude of reflector as the reference for calculation purposes;
- Calculate the Azimuth and Elevation of the normal to the reflector;
- Calculate the 3D angle between the source and the normal;
- If this angle is less than 90 degrees a reflection will occur. If it is greater than 90 degrees no reflection will occur because the source is behind the reflector;
- Calculate the Azimuth and Elevation of the reflection in accordance with the following:
  - The angle between source and normal is equal to angle between normal and reflection;
  - Source, Normal and Reflection are in the same plane.

## APPENDIX F – ASSESSMENT LIMITATIONS AND ASSUMPTIONS

### Pager Power's Model

The model considers 100% sunlight during daylight hours which is highly conservative.

The model does not account for terrain between the reflecting solar panels and the assessed receptor where a solar reflection is geometrically possible.

The model considers terrain between the reflecting solar panels and the visible horizon (where the sun may be obstructed from view of the panels)<sup>38</sup>.

It is assumed that the panel elevation angle assessed represents the elevation angle for all of the panels within each solar panel area defined.

It is assumed that the panel azimuth angle assessed represents the azimuth angle for all of the panels within each solar panel area defined.

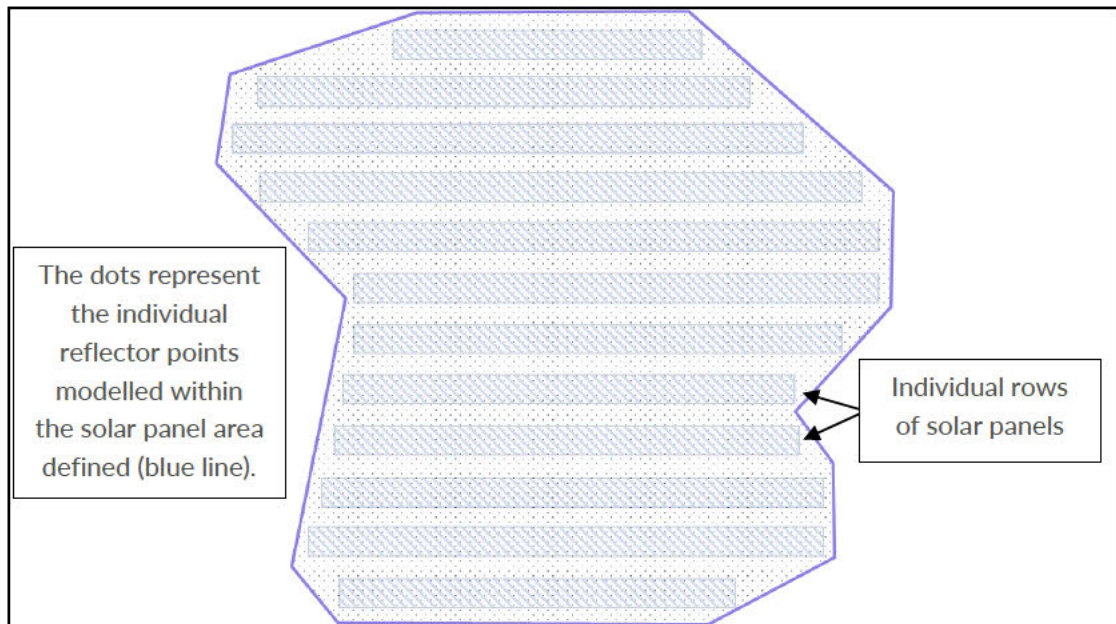
Only a reflection from the face of the panel has been considered. The frame or the reverse or frame of the solar panel has not been considered.

The model assumes that a receptor can view the face of every panel (point, defined in the following paragraph) within the development area whilst in reality this, in the majority of cases, will not occur. Therefore any predicted solar reflection from the face of a solar panel that is not visible to a receptor will not occur in practice.

A finite number of points within each solar panel area defined is chosen based on an assessment resolution so that a comprehensive understanding of the entire development can be formed. This determines whether a solar reflection could ever occur at a chosen receptor. The model does not consider the specific panel rows or the entire face of the solar panel within the development outline, rather a single point is defined every 'x' metres (based on the assessment resolution) with the geometric characteristics of the panel. A panel area is however defined to encapsulate all possible panel locations. See the figure below which illustrates this process.

---

<sup>38</sup> UK only.



*Solar panel area modelling overview*

A single reflection point is chosen for the geometric calculations. This suitably determines whether a solar reflection can be experienced at a receptor location and the time of year and duration of the solar reflection. Increased accuracy could be achieved by increasing the number of heights assessed however this would only marginally change the results and is not considered significant.

The available street view imagery, satellite mapping, terrain and any site imagery provided by the developer has been used to assess line of sight from the assessed receptors to the modelled solar panel area, unless stated otherwise. In some cases, this imagery may not be up to date and may not give the full perspective of the installation from the location of the assessed receptor.

Any screening in the form of trees, buildings etc. that may obstruct the Sun from view of the solar panels is not within the modelling unless stated otherwise. The terrain profile at the horizon is considered if stated.

## Forge's Sandia National Laboratories' (SGHAT) Model<sup>39</sup>

Summary of assumptions and abstractions required by the SGHAT/ForgeSolar analysis methodology

1. Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.
2. Result data files and plots are now retained for two years after analysis completion. Files should be downloaded and saved if additional persistence is required.
3. The algorithm does not rigorously represent the detailed geometry of a system; detailed features such as gaps between modules, variable height of the PV array, and support structures may impact actual glare results. However, we have validated our models against several systems, including a PV array causing glare to the air-traffic control tower at Manchester-Boston Regional Airport and several sites in Albuquerque, and the tool accurately predicted the occurrence and intensity of glare at different times and days of the year.
4. Several calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for large PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare. This primarily affects analyses of path receptors.
5. Random number computations are utilized by various steps of the annual hazard analysis algorithm. Predicted minutes of glare can vary between runs as a result. This limitation primarily affects analyses of Observation Point receptors, including ATCTs. Note that the SGHAT/ForgeSolar methodology has always relied on an analytical, qualitative approach to accurately determine the overall hazard (i.e. green vs. yellow) of expected glare on an annual basis.
6. The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)
7. The algorithm assumes that the PV array is aligned with a plane defined by the total heights of the coordinates outlined in the Google map. For more accuracy, the user should perform runs using minimum and maximum values for the vertex heights to bound the height of the plane containing the solar array. Doing so will expand the range of observed solar glare when compared to results using a single height value.
8. The algorithm does not consider obstacles (either man-made or natural) between the observation points and the prescribed solar installation that may obstruct observed glare, such as trees, hills, buildings, etc.
9. The variable direct normal irradiance (DNI) feature (if selected) scales the user-prescribed peak DNI using a typical clear-day irradiance profile. This profile has a lower DNI in the mornings and evenings and a maximum at solar noon. The scaling uses a clear-day irradiance profile based on a normalized time relative to sunrise, solar noon, and sunset, which are prescribed by a sun-position algorithm and the latitude and longitude obtained from Google maps. The actual DNI on any given day can be affected by cloud cover, atmospheric attenuation, and other environmental factors.
10. The ocular hazard predicted by the tool depends on a number of environmental, optical, and human factors, which can be uncertain. We provide input fields and typical ranges of values for these factors so that the user can vary these parameters to see if they have an impact on the results. The speed of SGHAT allows expedited sensitivity and parametric analyses.
11. The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.
12. Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.
13. Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.
14. Glare vector plots are simplified representations of analysis data. Actual glare emanations and results may differ.
15. PV array tracking assumes the modules move instantly when tracking the sun, and when reverting to the rest position.

---

<sup>39</sup> <https://www.forgesolar.com/help/#assumptions>

**PAGERPOWER**   
Urban & Renewables

**Pager Power Limited**  
Stour Valley Business Centre  
Sudbury  
Suffolk  
CO10 7GB

**Tel:** +44 1787 319001 **Email:** [info@pagerpower.com](mailto:info@pagerpower.com) **Web:** [www.pagerpower.com](http://www.pagerpower.com)

# APPENDIX F: PRELIMINARY ECOLOGICAL APPRAISAL (DEVELOPABLE AREAS) [CONFIDENTIAL]

---

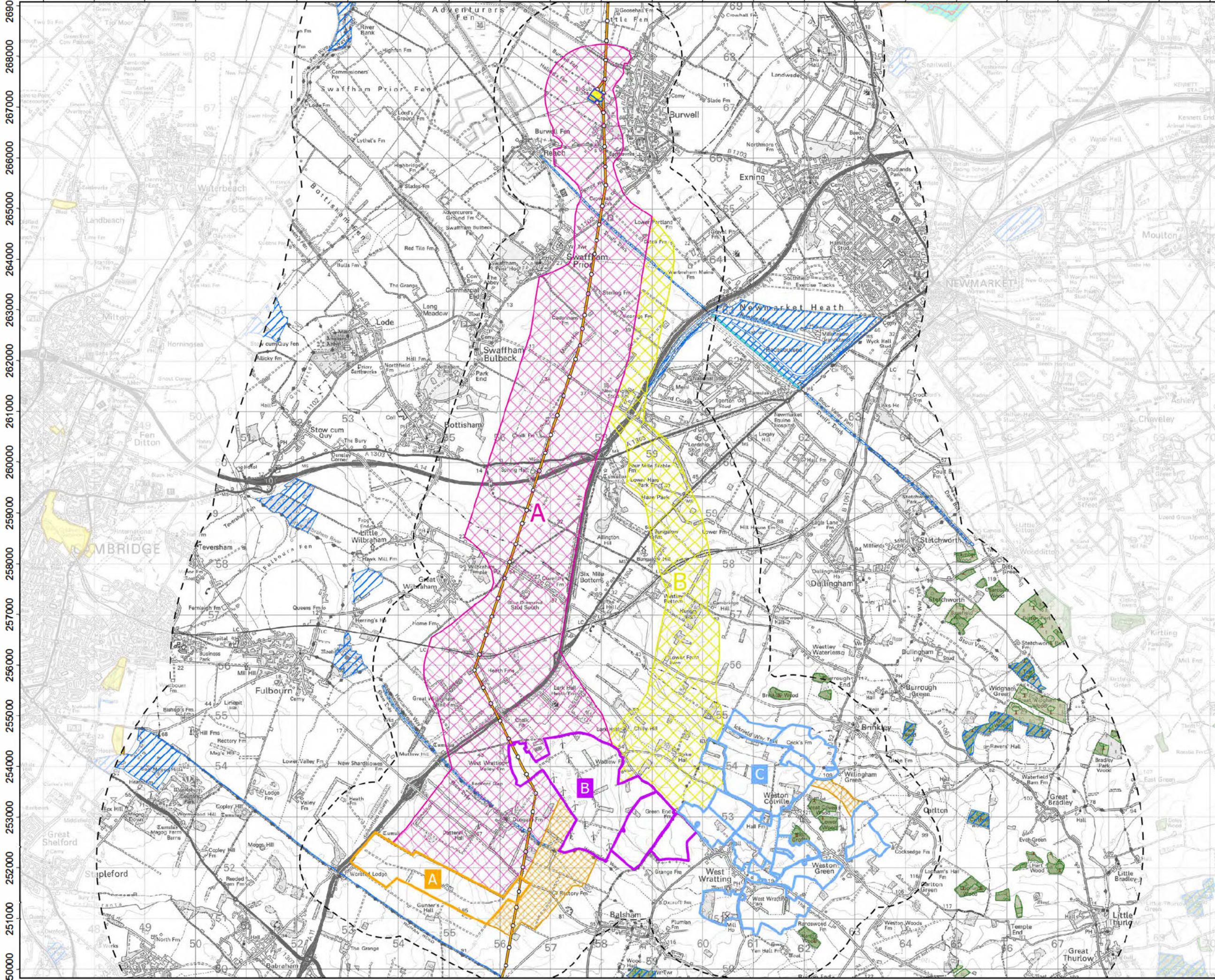
**NOTE:** This report is confidential because of sensitive species location information.



## APPENDIX G: BIODIVERSITY FIGURE

---

547000 548000 549000 550000 551000 552000 553000 554000 555000 556000 557000 558000 559000 560000 561000 562000 563000 564000 565000 566000 567000 568000 569000 570000



**Legend:**  
**Scheme Components and Existing infrastructure**  
 Kingsway Solar farm Site Boundary  
 Area A, West  
 Area B, Central  
 Area C, East  
 Inter Array Connection Corridors  
 Grid Connection Corridor A  
 Grid Connection Corridor B  
 1km and 5km Component Boundary  
 Buffers  
 National Grid Substations  
 National Grid Towers  
 National Grid OHL  
**Ecology Features**  
 Ramsar  
 Local Nature Reserves  
 National Nature Reserves  
 Sites of Special Scientific Interest  
 Special Areas of Conservation  
**Ancient Woodland**  
 Ancient & Semi-Natural Woodland  
 Ancient Replanted Woodland

*There are no Special Protection Areas present in the extent of this figure.*  
 Coordinate System: British National Grid  
 Projection: Transverse Mercator  
 Datum: OSGB 1936  
 Units: Meter



Rev	Date	Description	Drn	Chk	App
00	28/10/2024	First Issue	CJ	CP	CP

**Kingsway Solar Farm**

TITLE: Biodiversity Features  
 ID: Biodiversity\_features\_A3L

